



# Input Data

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# In This Session ...

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- Discuss input data required for 3D frac models
- Introduce the complete stress equation as implemented in GOHFER
- Break apart the elements of the stress equation
  - Poisson's Ratio and Young's Modulus
  - Net Effective Stress
    - Pore Pressure, Overburden Pressure, Biot's Constant
  - External Stress Boundary Conditions
- Height Containment Mechanisms other than Stress Contrast



# Types of Input Data

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- Control of **Stress Profile**
  - Poisson's Ratio
  - Young's Modulus
  - Stress and Strain Offsets
  - Pore Pressure
  - Biot's Alpha
  - Depth
  - OB Gradient
- Control of Fracture Growth
  - **Stress Profile**
  - Process Zone Stress

Other input data relating to fluid loss and efficiency, fluid and solid transport, and post frac production will be discussed later.



# Definition of Stress and Pressure

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- Stress and pressure are both terms for the magnitude of an applied force per unit area ( $\text{lb}_f/\text{in}^2$ , Pa, bar, atm,  $\text{kg}/\text{m}^2$ , etc.)
- the term “pressure” is applied to fluids
  - Pressure acts equally in all directions
  - Pressure has magnitude only
- The term “stress” is applied to solids
  - Stress has direction and magnitude
  - Stress is considered to be a vector or tensor quantity
  - Stress is not isotropic
  - Positive stresses lead to compression and negative stresses to extension



# *In Situ* Earth Stresses

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- Stresses caused by overburden weight
  - Vertical to horizontal transform through confined compaction
- Stresses caused by tectonic movements
- Stresses caused by creep-flow and plasticity
- Effects of pore pressure and its variation
- Stresses caused by diagenesis

Obtain elastic properties from core and logs

Infer all other influences from field measurements



# GOHFER's

## Complete Stress Equation

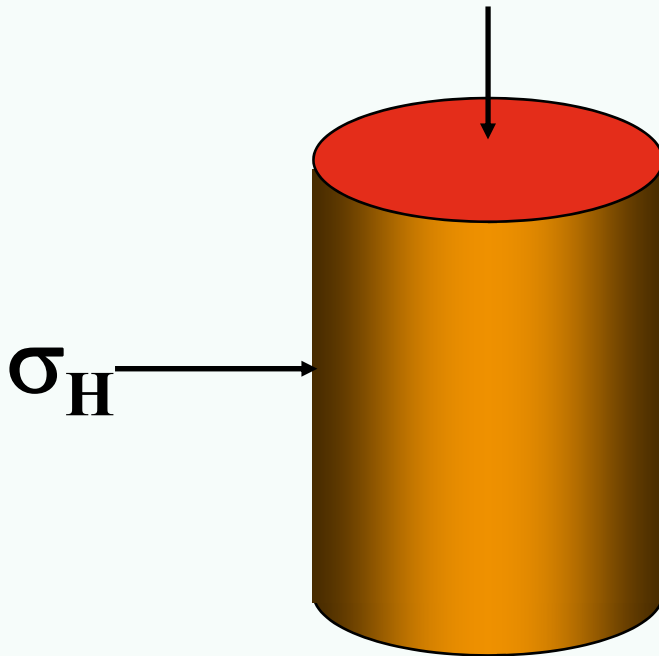
$$P_c = \frac{\nu}{(1-\nu)} [P_{ob} - \alpha_v P_p] + \alpha_h P_p + \varepsilon_x E + \sigma_t$$

- $P_c$  = closure pressure, psi
- $\nu$  = Poisson's Ratio
- $P_{ob}$  = Overburden Pressure
- $\alpha_v$  = vertical Biot's poroelastic constant
- $\alpha_h$  = horizontal Biot's poroelastic constant
- $P_p$  = Pore Pressure
- $\varepsilon_x$  = regional horizontal strain, microstrains
- $E$  = Young's Modulus, million psi
- $\sigma_t$  = regional horizontal tectonic stress



# Uniaxial Strain: Deformation in One Direction

$$\sigma_v = P_{OB} - \alpha P_P$$



**Horizontal stress  
required to assure no  
lateral strain**

$$\sigma_H = (P_{OB} - \alpha P_P) \frac{\nu}{(1 - \nu)}$$



# Overburden Pressure

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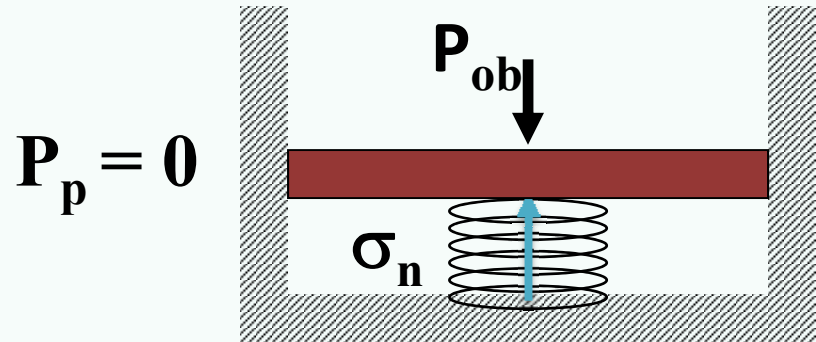
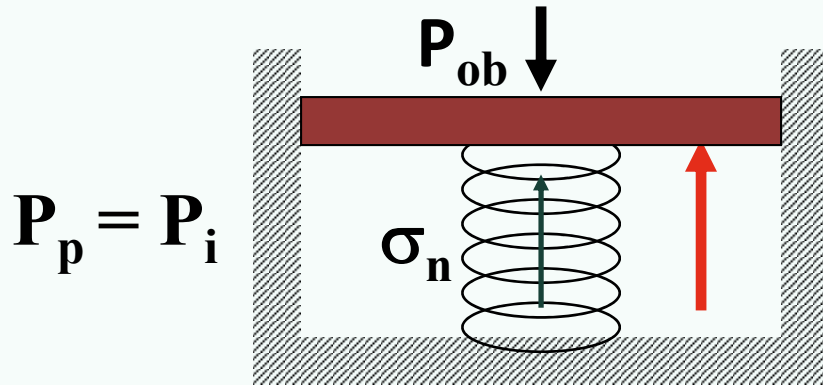
- $P_{ob}$  is the externally applied load
- In GOHFER expressed by:
  - $D_{tv}\gamma_{ob}$
  - Where
    - $\gamma_{ob}$  is the overburden stress gradient, psi/ft
    - $D_{tv}$  is the true vertical depth, feet





# Net Stress Causes Rock Deformation

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- *Total Stress Remains Constant*
- *As pore pressure declines, net stress increases*
  - $\sigma_n = P_{ob} - \alpha P_p$

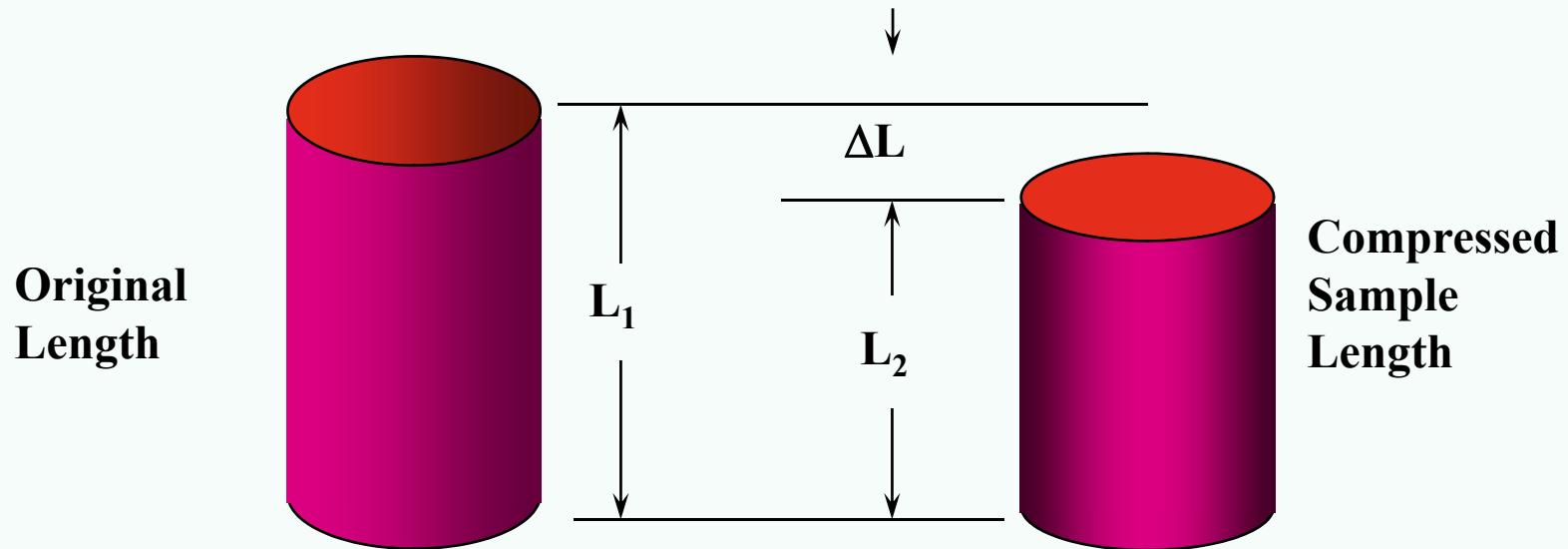


# Definition of Strain

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$$\text{Strain} = \frac{\text{Change in Length}}{\text{Original Length}}$$

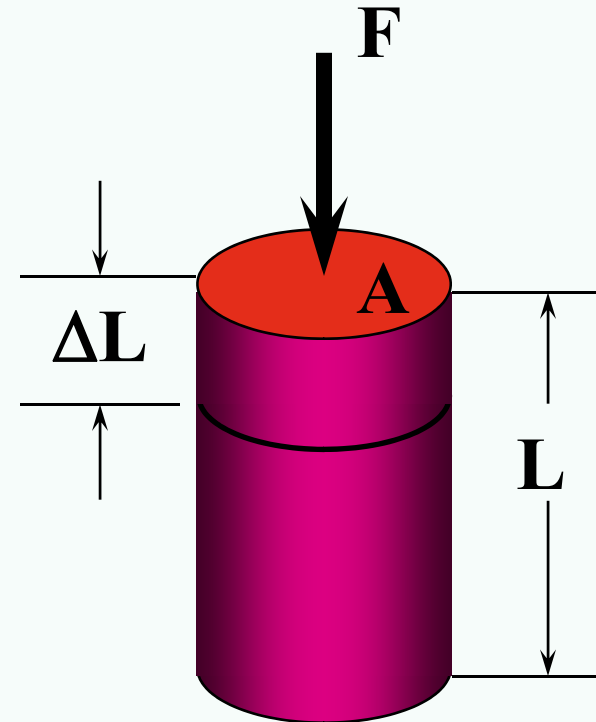
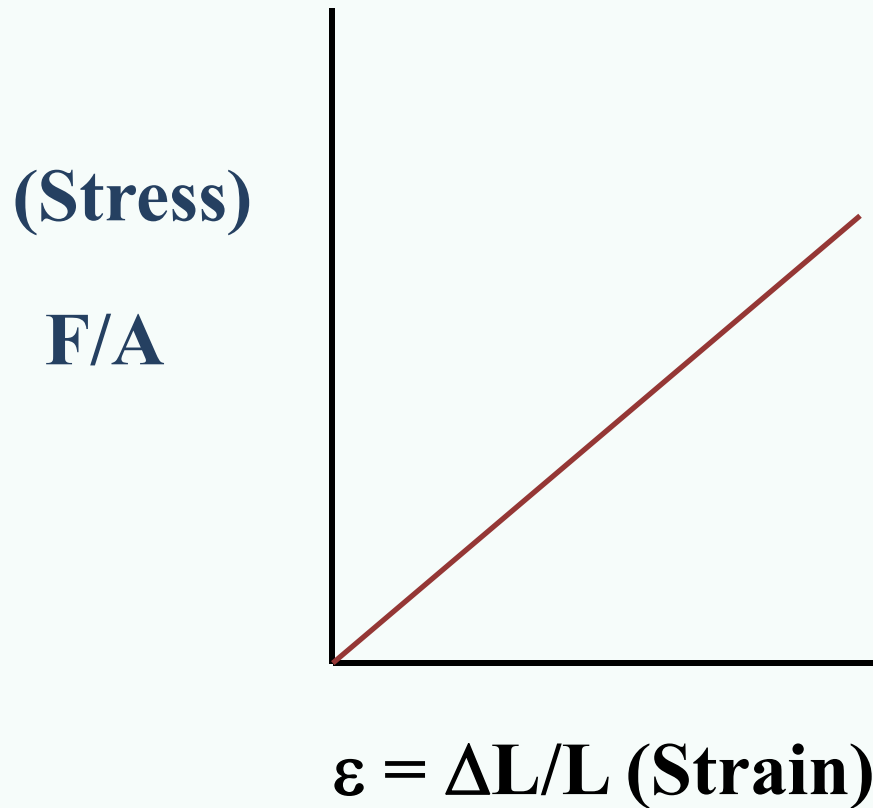
$$\varepsilon = \frac{L_2 - L_1}{L_1} = \frac{\Delta L}{L}$$





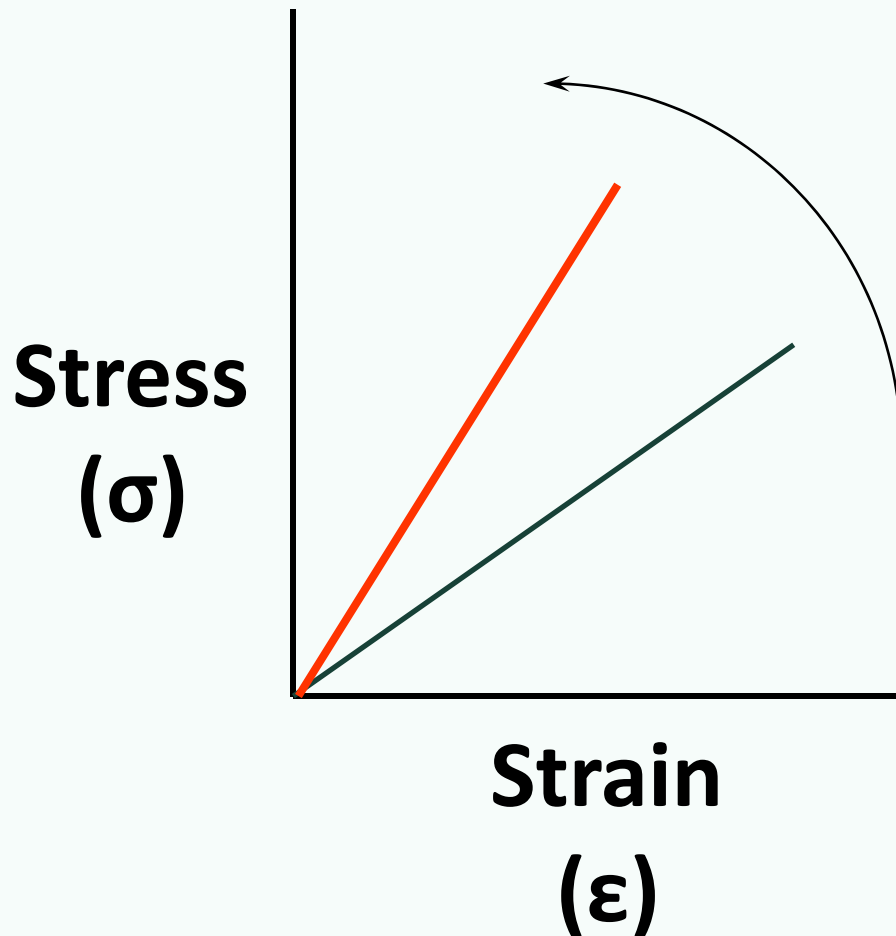
# Stress/Strain Relationship

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# Stress/Strain Slope – Rock Stiffness

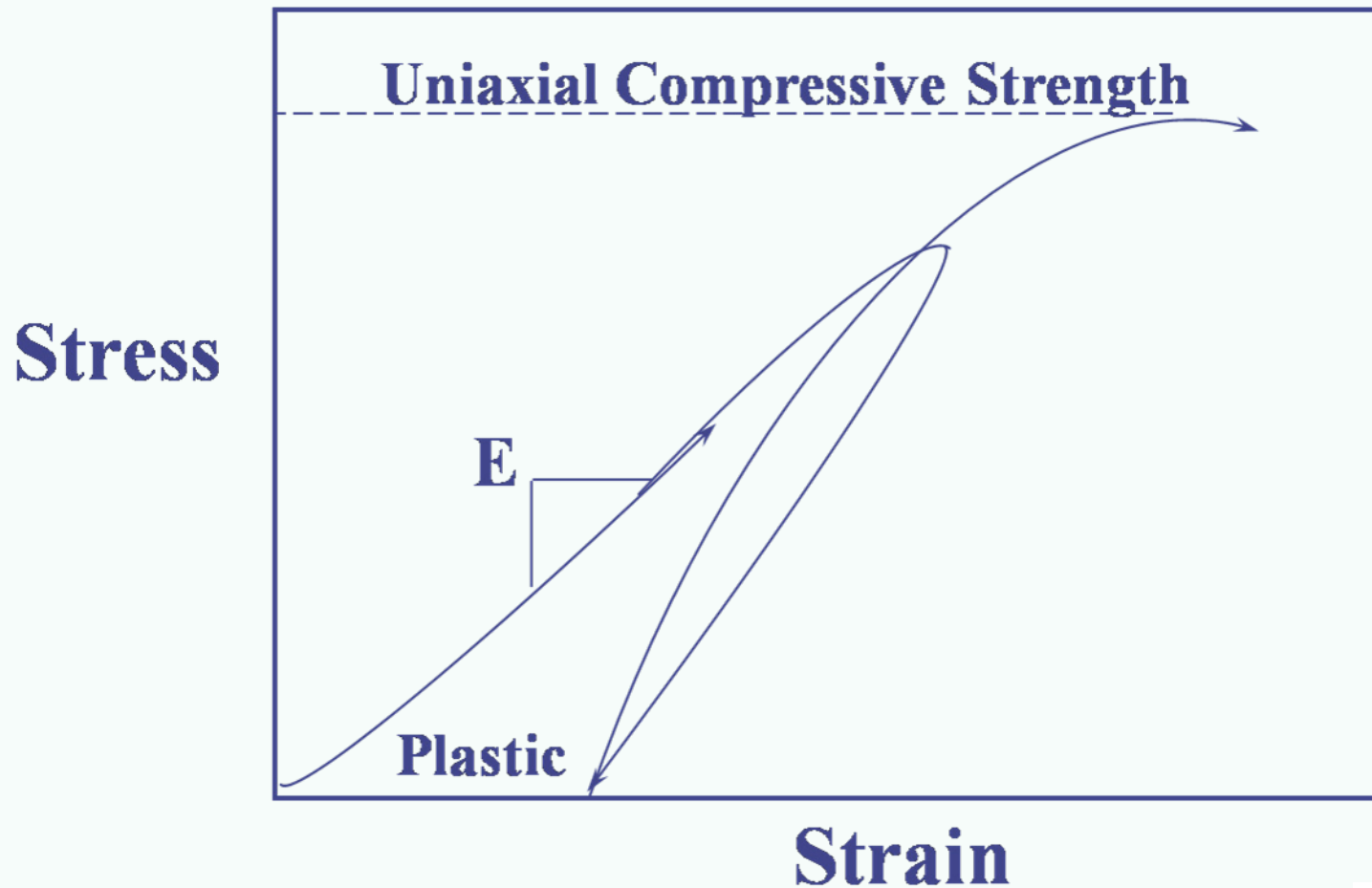
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- Young's Modulus:  
 $E = \sigma / \epsilon$
- Higher Slope Indicates Stiffer Material



# Young's Modulus is Not a Constant & Deformation is Non-Linear





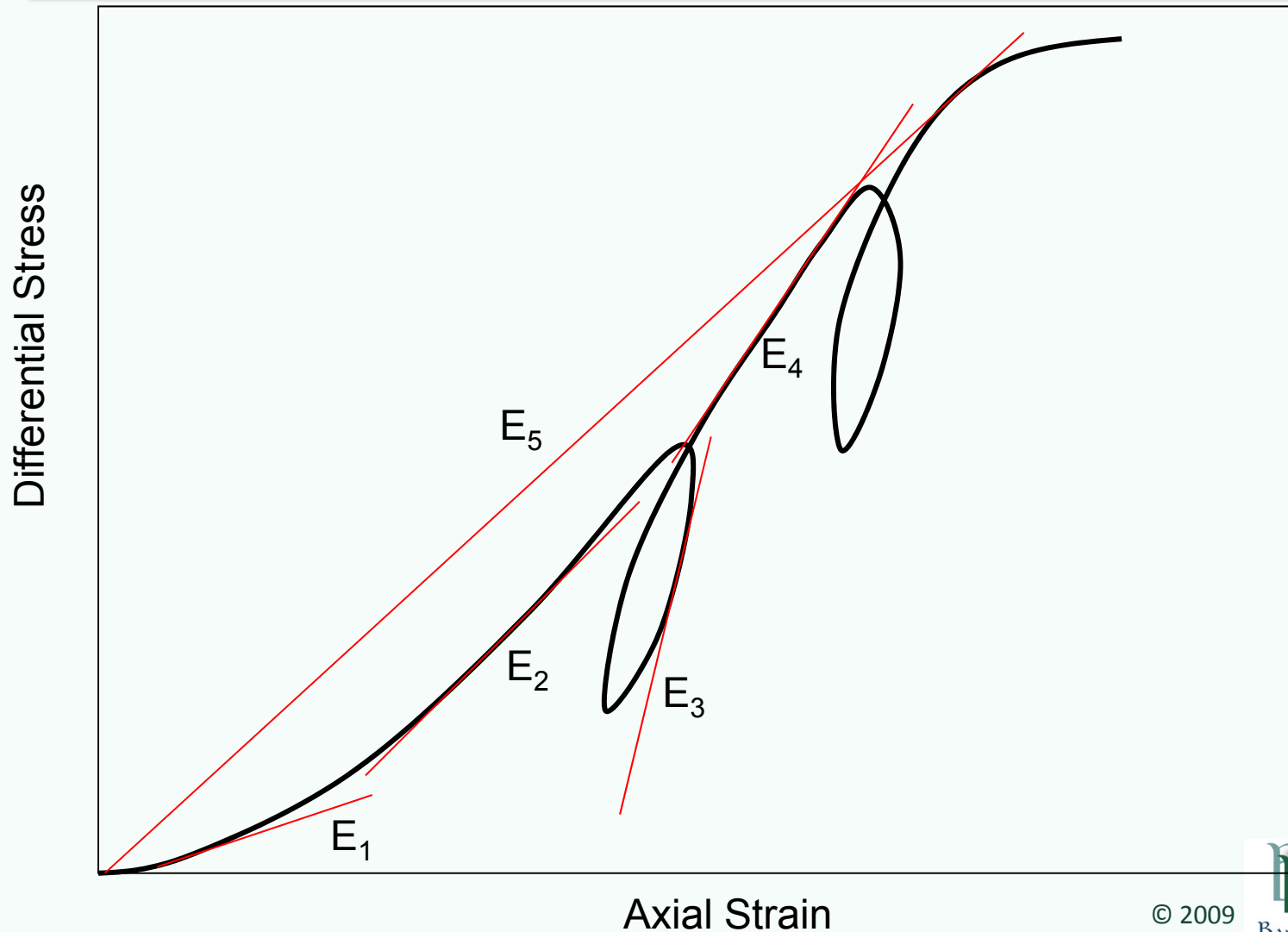
# Core Alteration During Coring and Handling

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- Removal of overburden stress while coring:
  - Core disking and fracturing
- Removal of confining stress during core recovery:
  - Expulsion of trapped pore pressure
  - Generation of microfractures
  - Anelastic strain (differential expansion) of core
- Thermal contraction
- Dessication and oxidation
- Stress cycling and non-representative stress states
- Improper restoration of saturation



# Modulus Depends on Conditions of Measurement

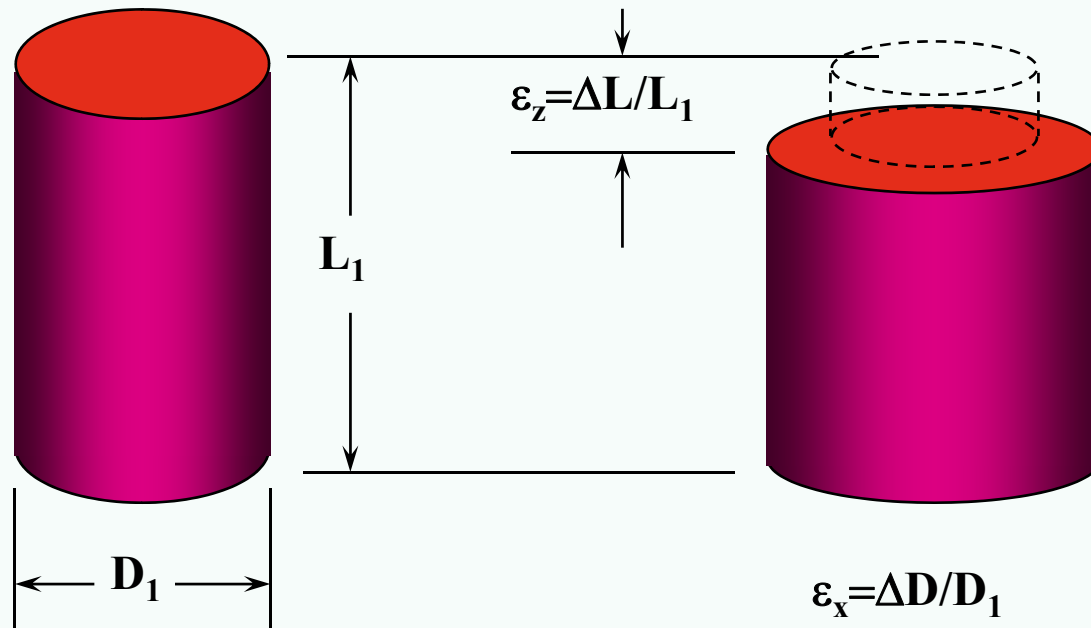




# Definition of Poisson's Ratio

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$$\text{Poisson's Ratio} = \nu = \epsilon_x / \epsilon_z$$



$$0 < \nu < 0.5$$





# Measurement of Dynamic and Static Elastic Properties

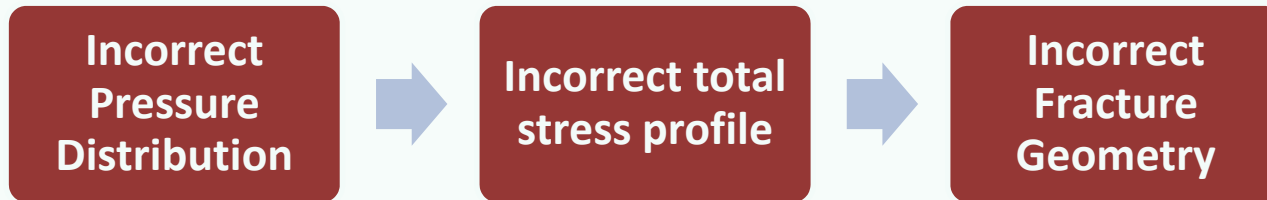
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- Dynamic modulus must be converted to static modulus
  - Static Modulus: large amplitude at low (zero) frequency (load frame tests)
  - Dynamic Modulus: small amplitude at high frequency (acoustic waves)
- Which stress state best defines the right conditions to measure modulus?
  - Results affected by strain rate, saturations, temperature, frequency, history, time, and many other factors



# Modeling of $P_p$ : Pore Pressure

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- Usual 'apparent' gradient gives pressure only at datum
- In the GOHFER total stress equation
  - expressed in more complex form
  - reflects change in pressure (and stress) across depth interval to be stimulated

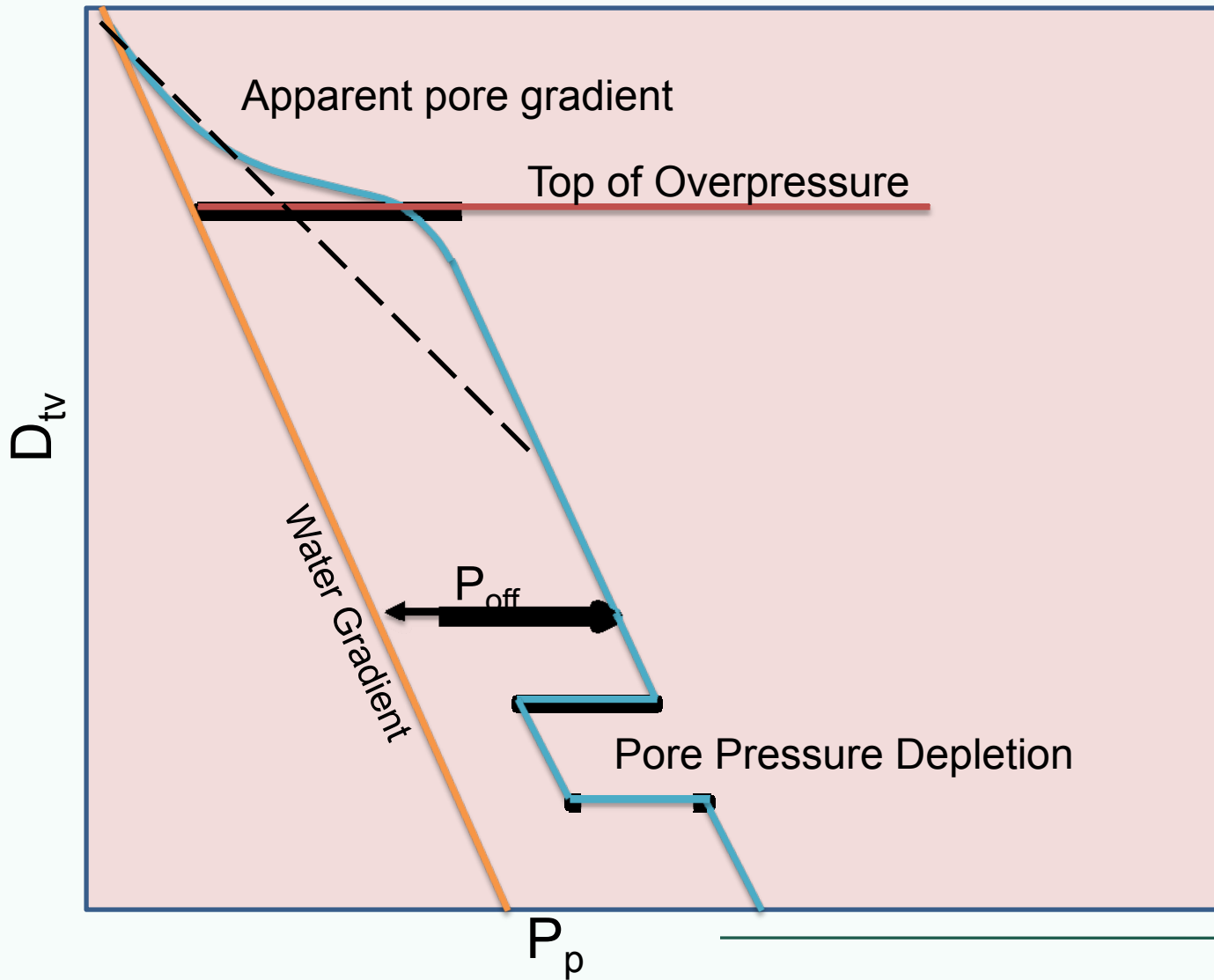
$$P_p = (D_{tv} \gamma_p + P_{off})$$

$D_{tv}$  = true vertical depth (feet)

$\gamma_p$  = pore fluid gradient, psi/ft

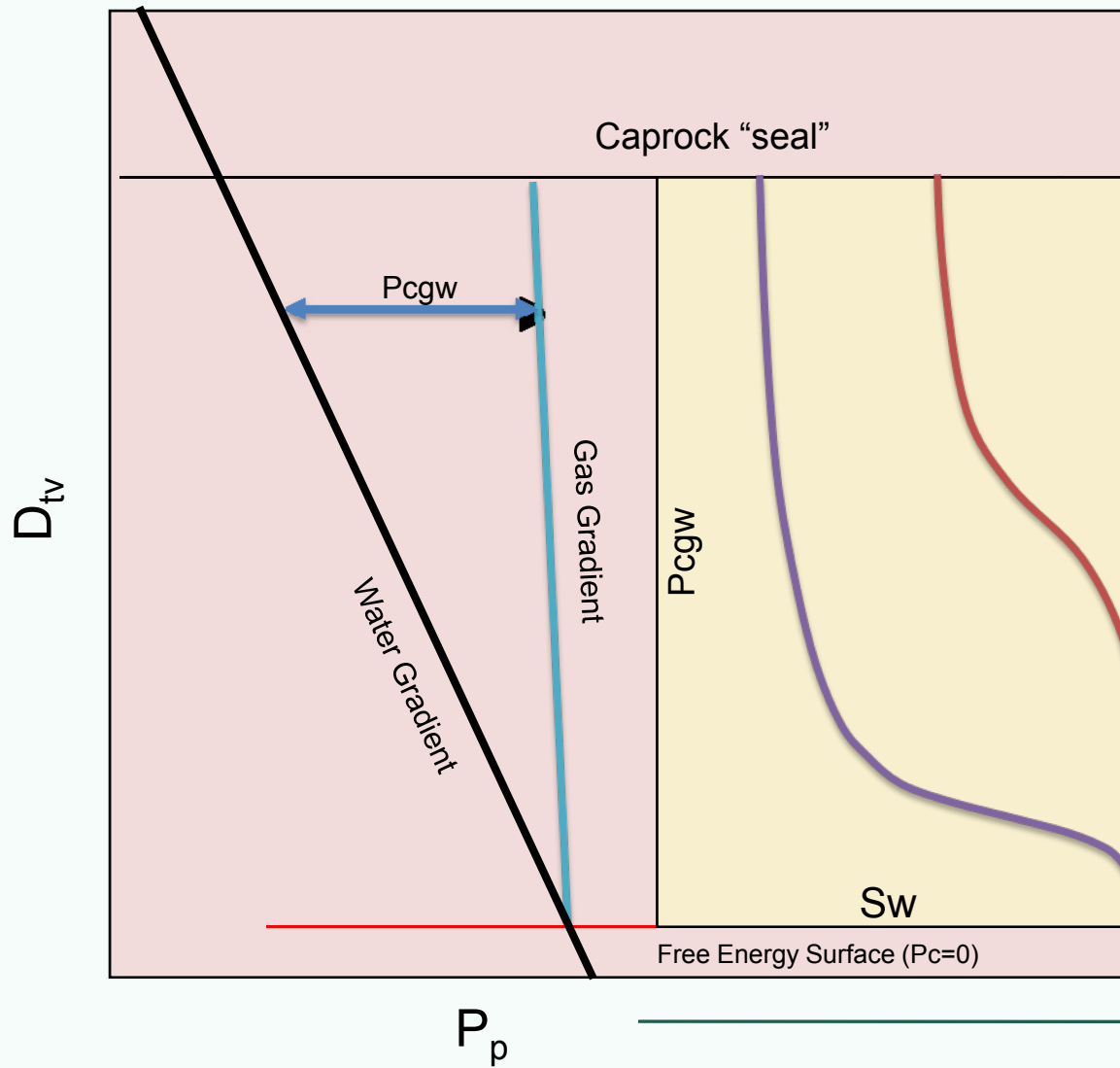
$P_{off}$  = pore pressure offset, psi

# Variable Pore Pressure Offset Geo Pressured Environment



# Variable Pore Pressure Offset

## Gravity-Capillary Pressure System





# Effect of Pore Pressure on Stress

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- Pore fluid supports part of the total stress
- Pore pressure depletion increases net stress and leads to compaction
- Pore pressure depletion decreases total (fracture closure) stress
- Fractures tend to grow into region of lowest pore pressure

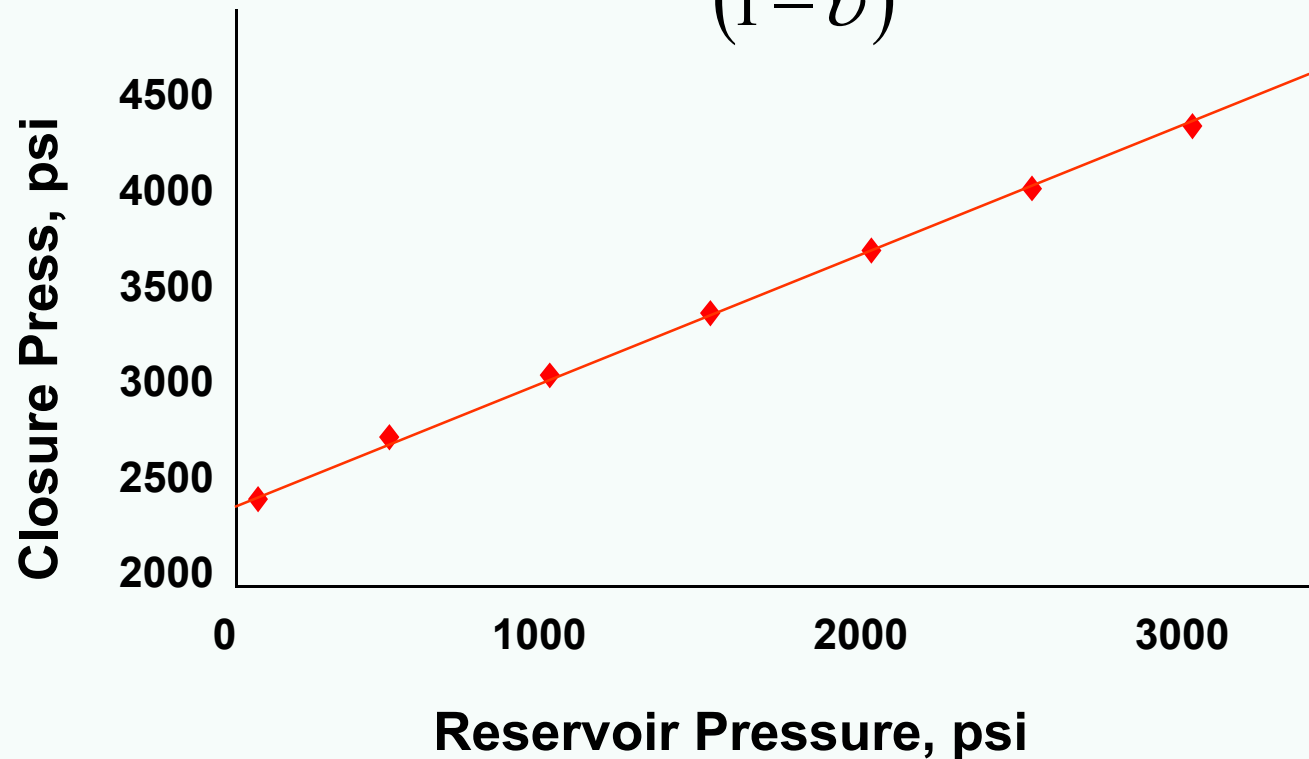


# Pore Pressure Variations Induce Closure Stress Contrasts

- Closure Pressure ( $P_c$ ) is affected by

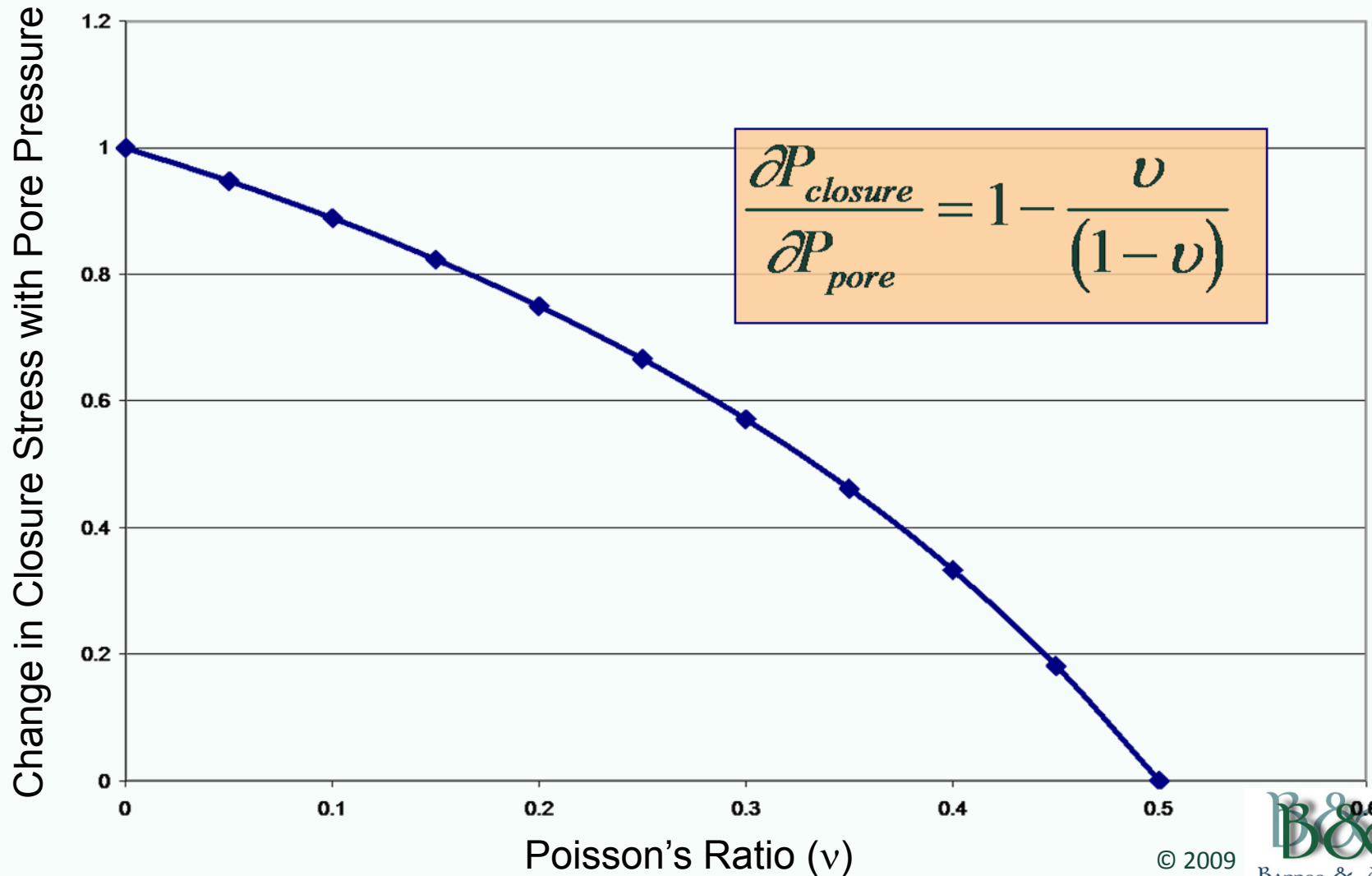
Pore Pressure ( $P_p$ ):

$$P_c = \frac{\nu}{(1-\nu)} (P_{ob} - \alpha P_p) + P_p + \sigma_x$$





# Closure Stress Change Related to Pressure Depletion and PR





# Reservoir Pressure Gradients

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- Fractures grow into areas of lower closure stress or pressure
  - vertical fracs grow upward in uniform rock
- Lateral pressure gradients have the same effect as vertical gradients
- Drilling and fracing in a pressure gradient can lead to asymmetric fracture growth





# What We Have So Far

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- So far we have transformed this:

$$\left[ P_{ob} - \alpha_v P_p \right] + \alpha_h P_p$$

- to

$$\left[ D_{tv} \gamma_{ob} - \alpha_v \left( D_{tv} \gamma_p + P_{off} \right) \right] + \alpha_h \left( D_{tv} \gamma_p + P_{off} \right)$$

So what about that  $\alpha$ ??



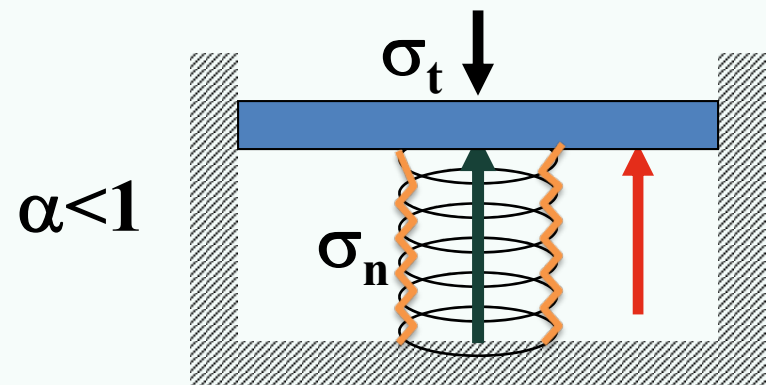
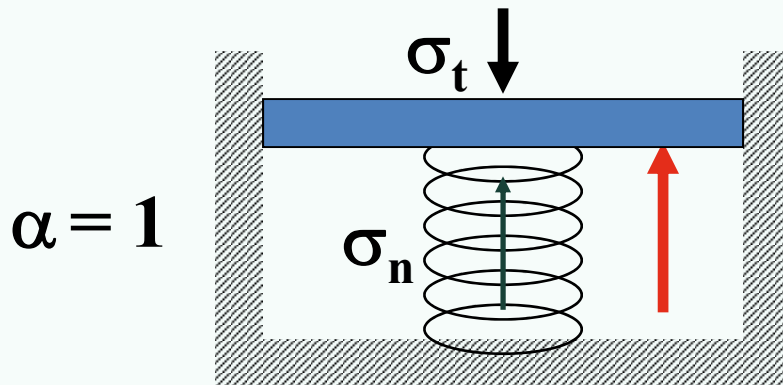
# Biot's Poroelastic Constant

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- Internal fluid pressure is not transmitted perfectly to the rock matrix
- Correction factor applied
  - Biot's poroelastic constant ( $\alpha$ )
- So net effective stress is:
  - $\sigma_n = P_{ob} - \alpha P_p$
  - *Which should make one part of the GOHFER equation recognizable as the net effective stress.*

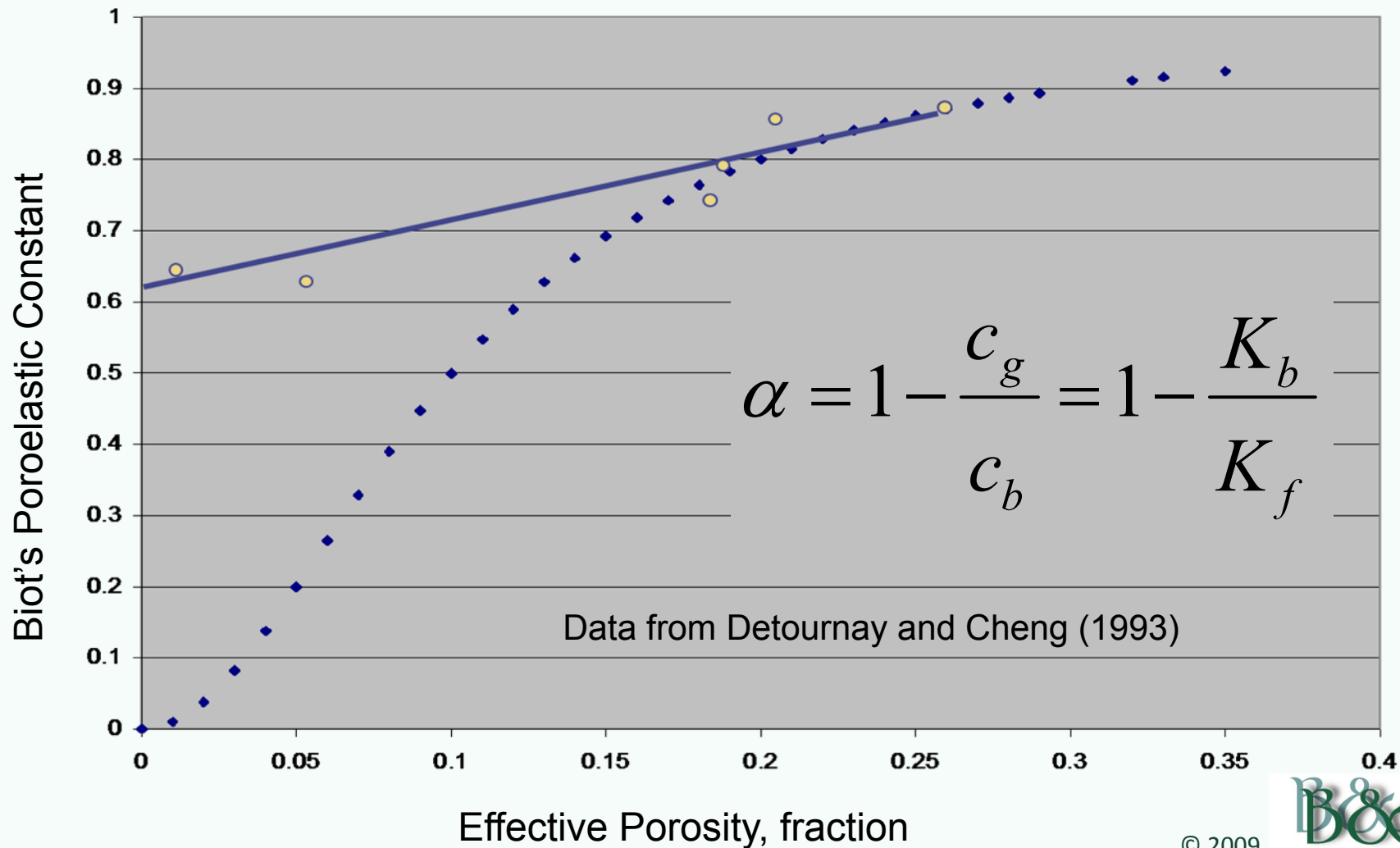
# Biot's Constant & Its Effects on Stress

- Biot's poroelastic constant ( $\alpha$ ) is the efficiency with which internal pore pressure offsets the externally applied vertical total stress
- as  $\alpha$  declines, net (intergranular) stress increases and pore pressure variations have less impact on net stress





# Possible Correlations for $\alpha$





# Assumptions in Stress Calculations

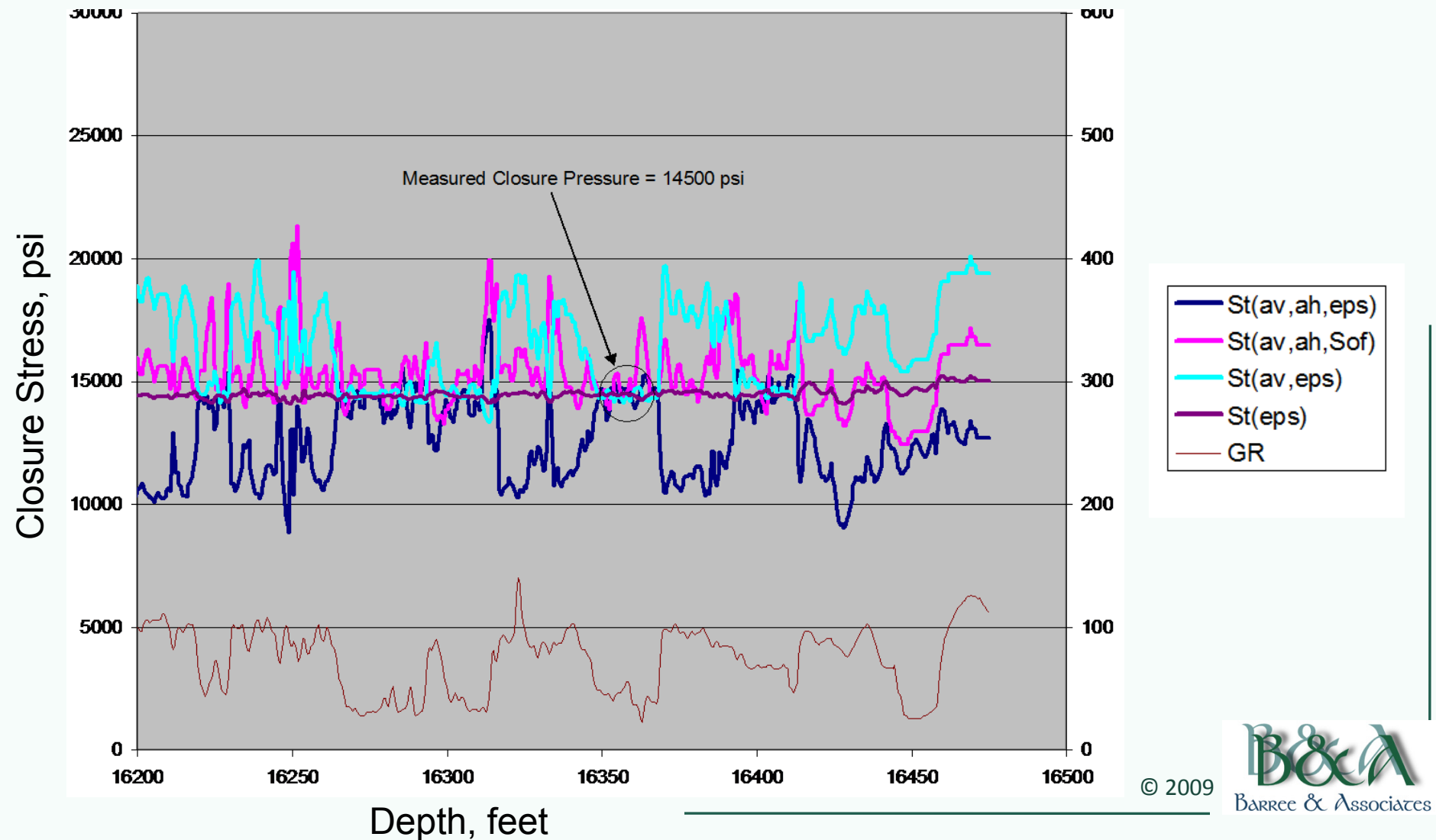
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$$P_c = \frac{\nu}{(1-\nu)} [P_{ob} - \alpha_v P_p] + \alpha_h P_p + \varepsilon_x E + \sigma_t$$

To calculate  $P_c$  assumptions must obviously be made about  $\alpha$  – possibilities include:

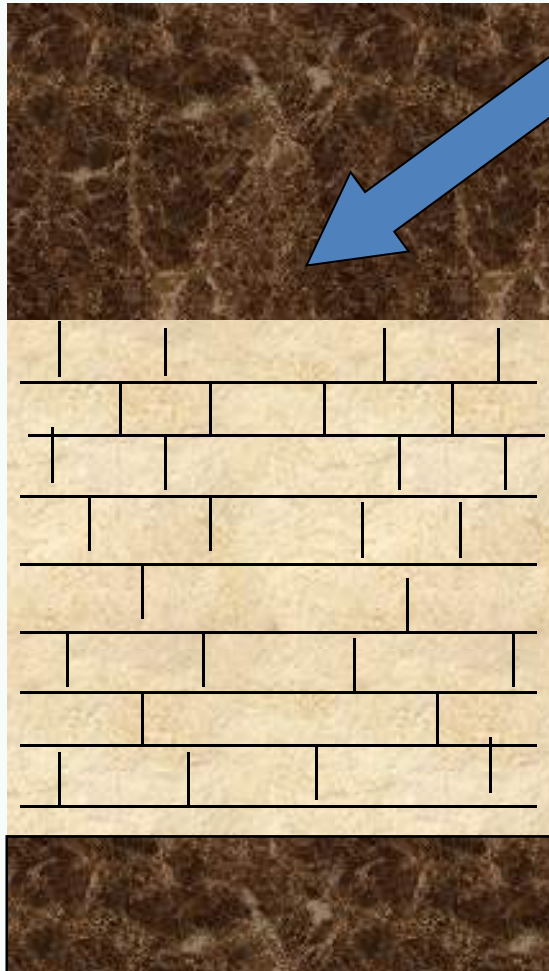
- $\alpha_v = \alpha_h$  f(PHIE), constant strain offset
- $\alpha_v = \alpha_h$  f(PHIE), constant stress offset
- $\alpha_v$  variable,  $\alpha_h=1$ , strain offset
- $\alpha_v = \alpha_h=1$ , strain offset

# Resulting Stress Profiles

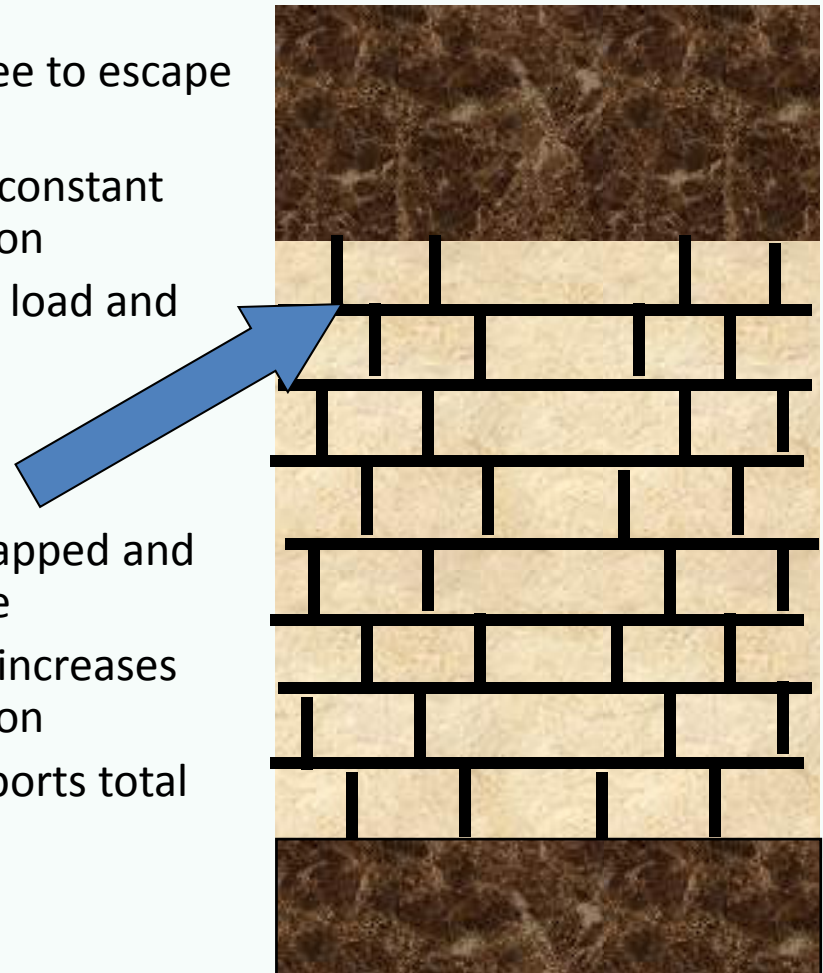




# Drained vs. Undrained Poisson's Ratio and Young's Modulus in Coals



- Drained Test:
  - Pore fluid is free to escape or compress
  - Pore pressure constant with compaction
  - Cleats support load and may shear
  - $\nu=0.35$
- Undrained Test:

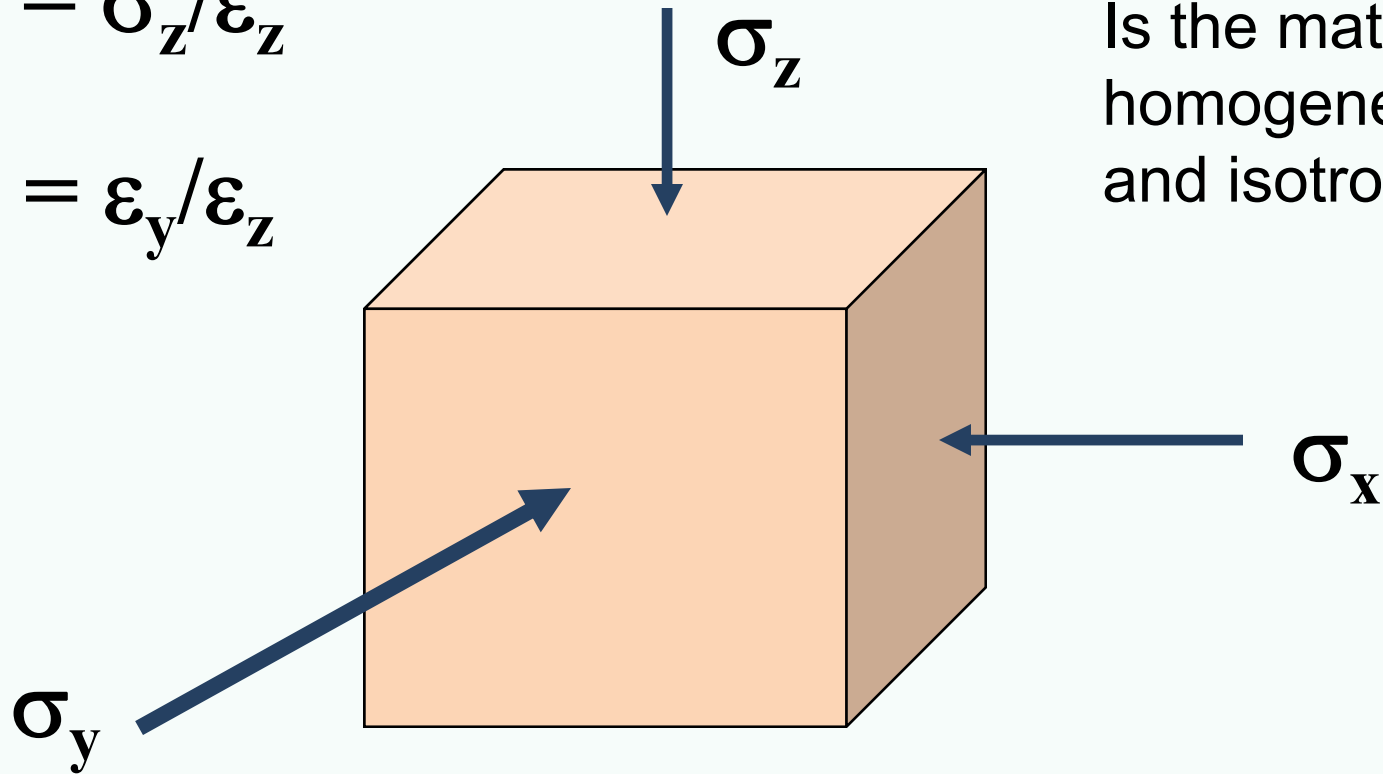


# Triaxial Loading:

## Defined by Three Principal Stresses

$$E = \sigma_z / \epsilon_z$$

$$\nu = \epsilon_y / \epsilon_z$$



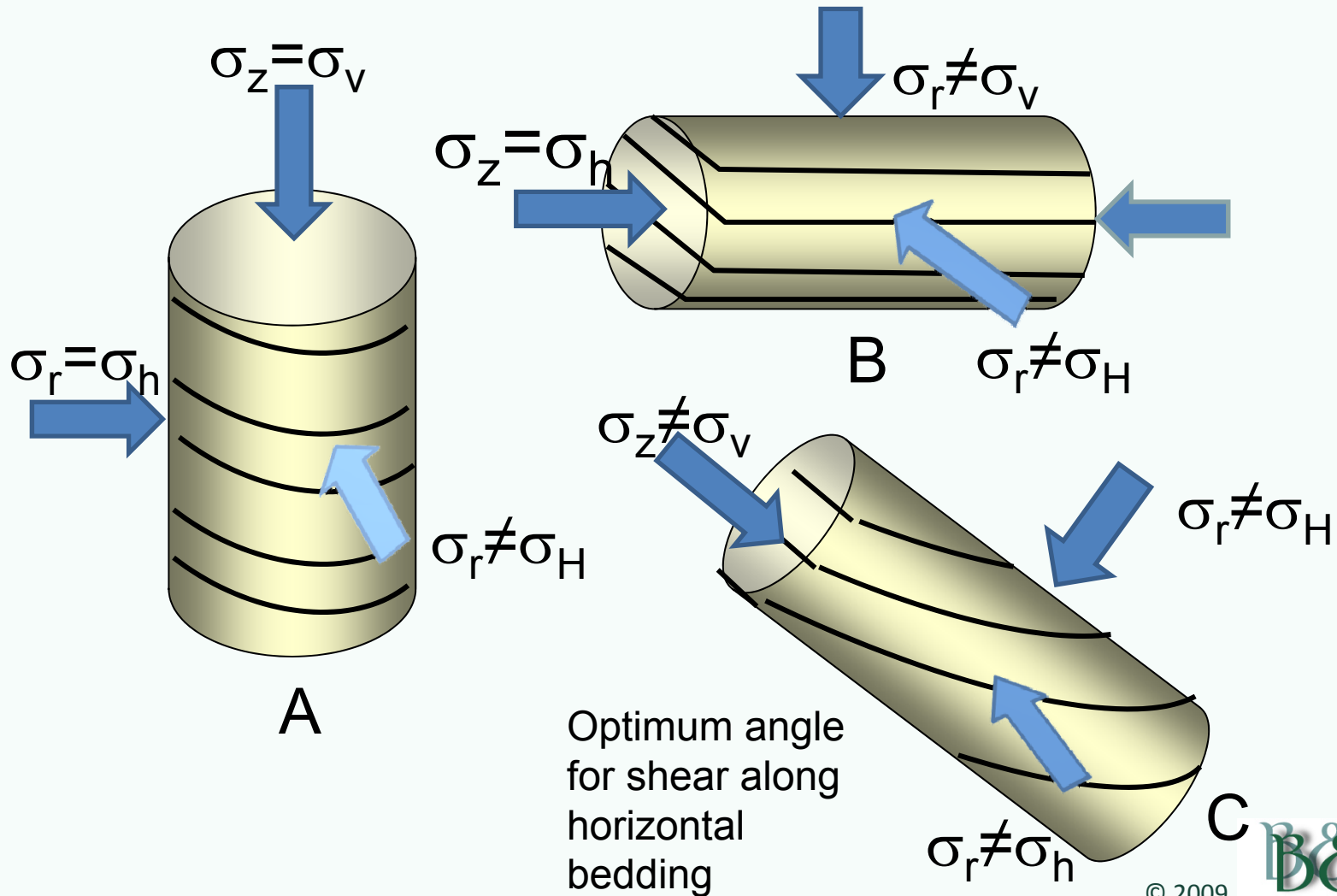
Is the material  
homogeneous  
and isotropic?





# Oriented Anisotropic Core Data: What does it mean?

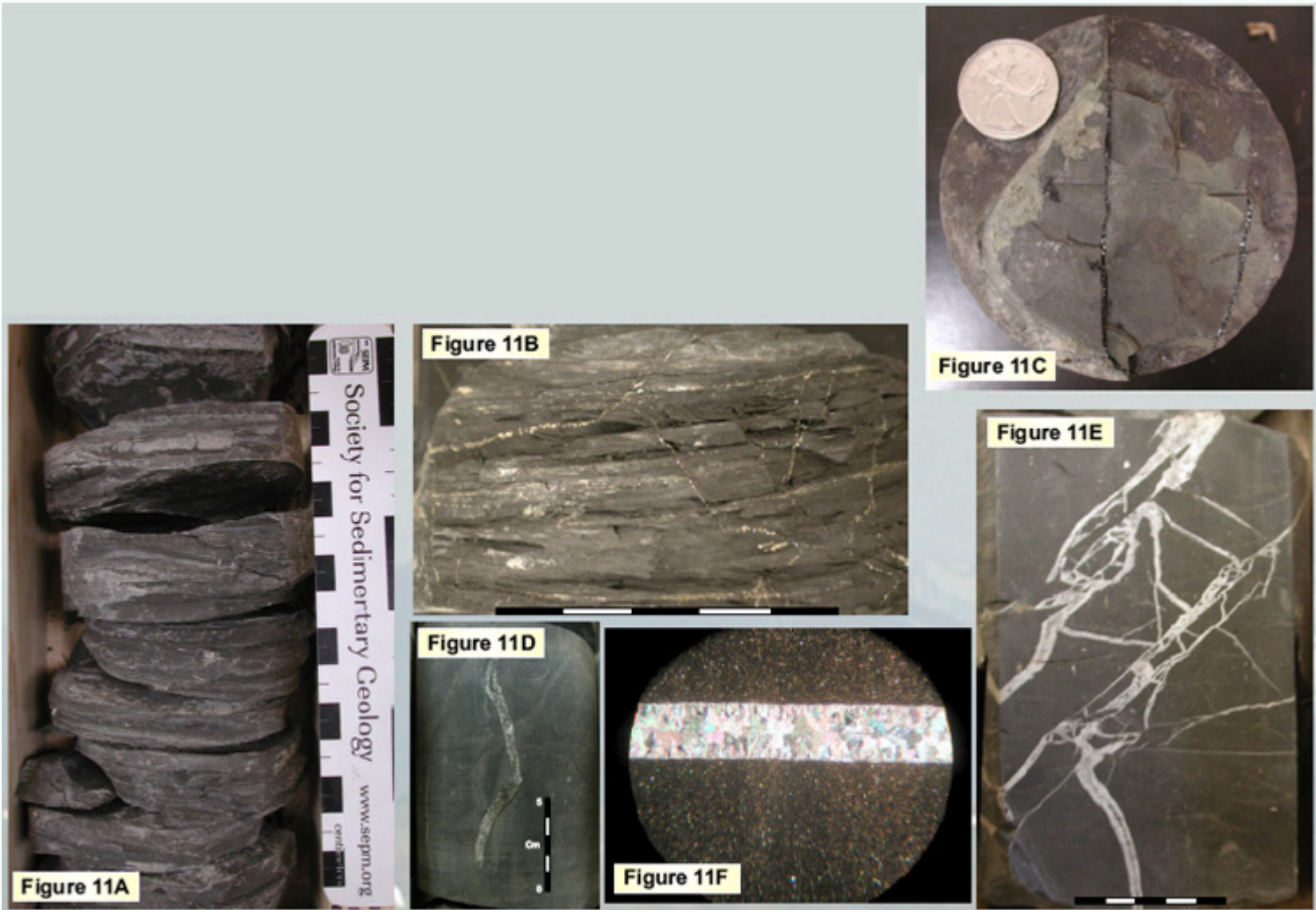
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# Fractures, Laminations, and Sample Scale Effects in Shale

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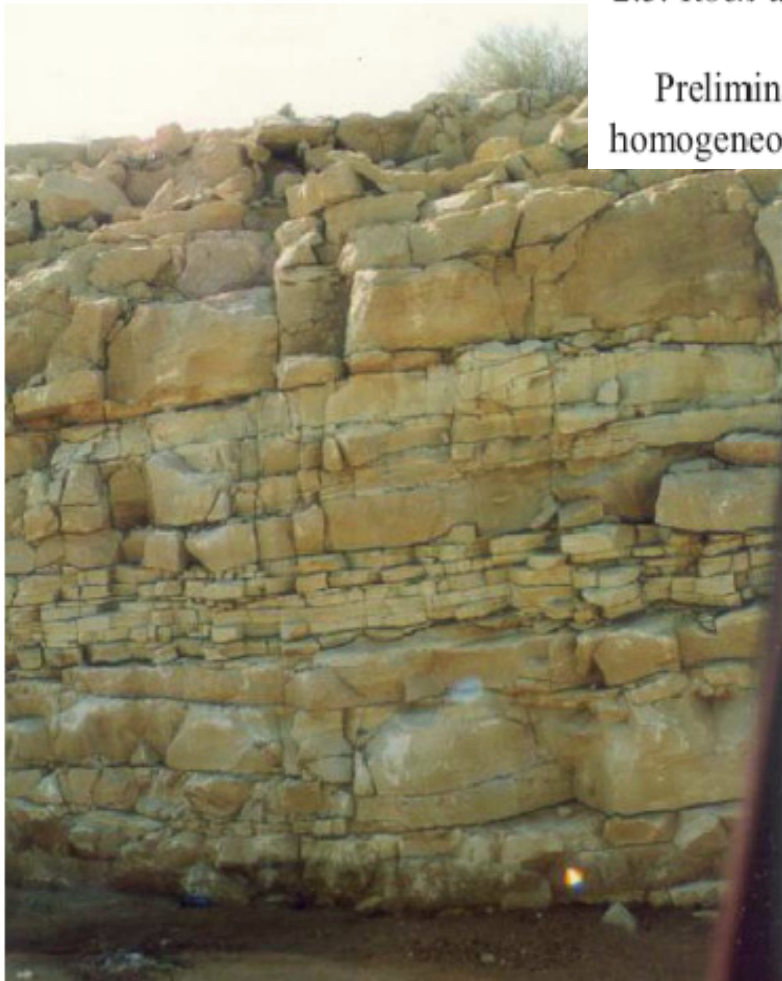


# Homogeneity and Anisotropy: What are we measuring?

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## *2.3. Rock description*

Preliminary studies showed that this rock is a very homogeneous, beige-colored, muddy limestone.







# What Are the Mechanical Properties of This?

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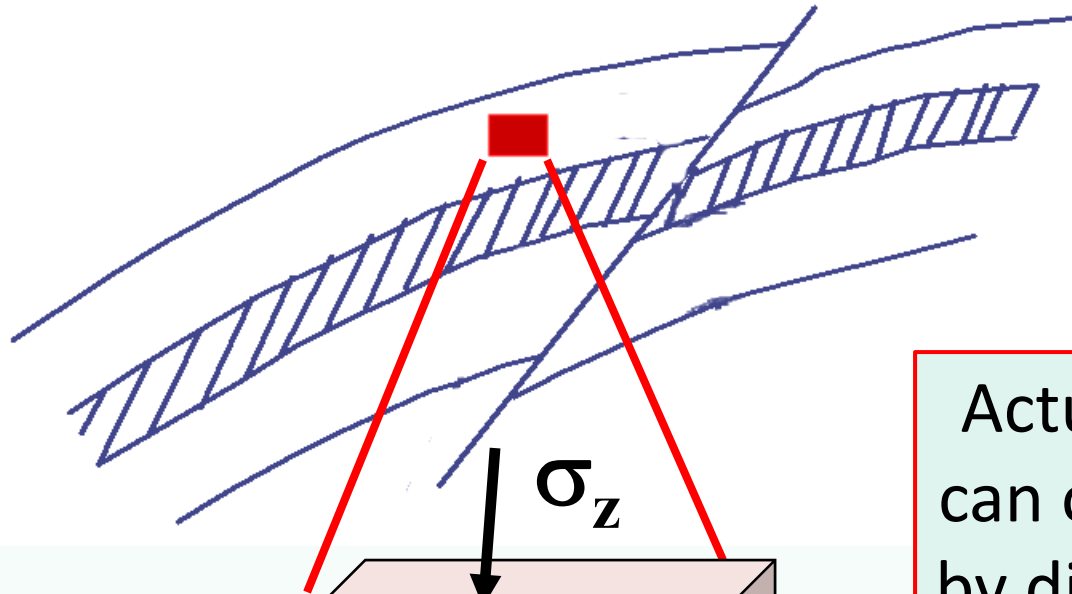


Photo credit: Alberta Geological Survey



# More Complex

## Realistic In-Situ Stress States



Actual in-situ stresses  
can only be determined  
by direct measurement.

$$\sigma_x \neq \sigma_y \neq \sigma_z$$

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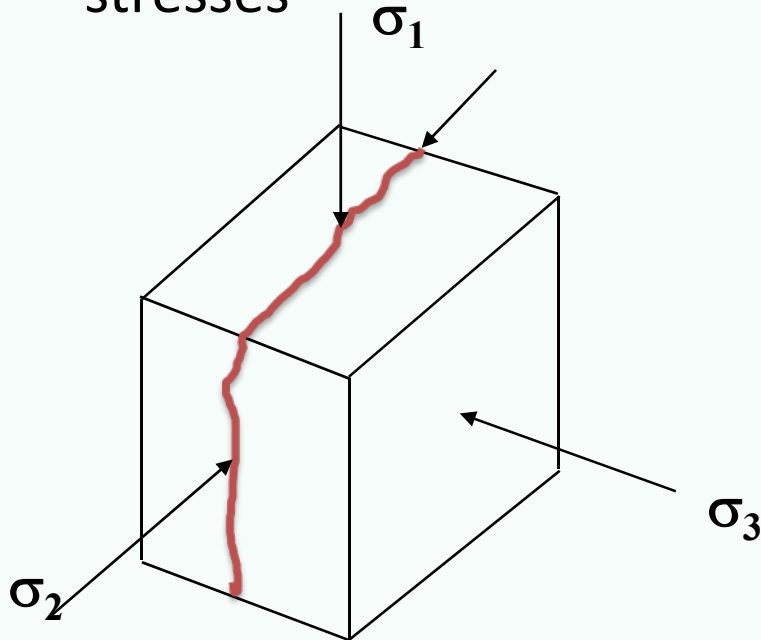


# In-Situ Stress Field Controls

## Fracture Orientation

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- Fracture orientation determined by relationship of principal stresses



- Stress distribution controls fracture orientation, height containment, treating pressure magnitude, and change in treating pressure during
- Orientation of induced fractures controlled primarily by the stress difference between the 3 principal stresses
- the major displacement (opening of fracture width) occurs in the direction of the minimum principal stress



# External Stress Boundary Conditions

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$$P_c = \frac{\nu}{(1-\nu)} [P_{ob} - \alpha_v P_p] + \alpha_h P_p + \underline{\underline{\varepsilon_x E + \sigma_t}}$$



# Handling Tectonic Stress

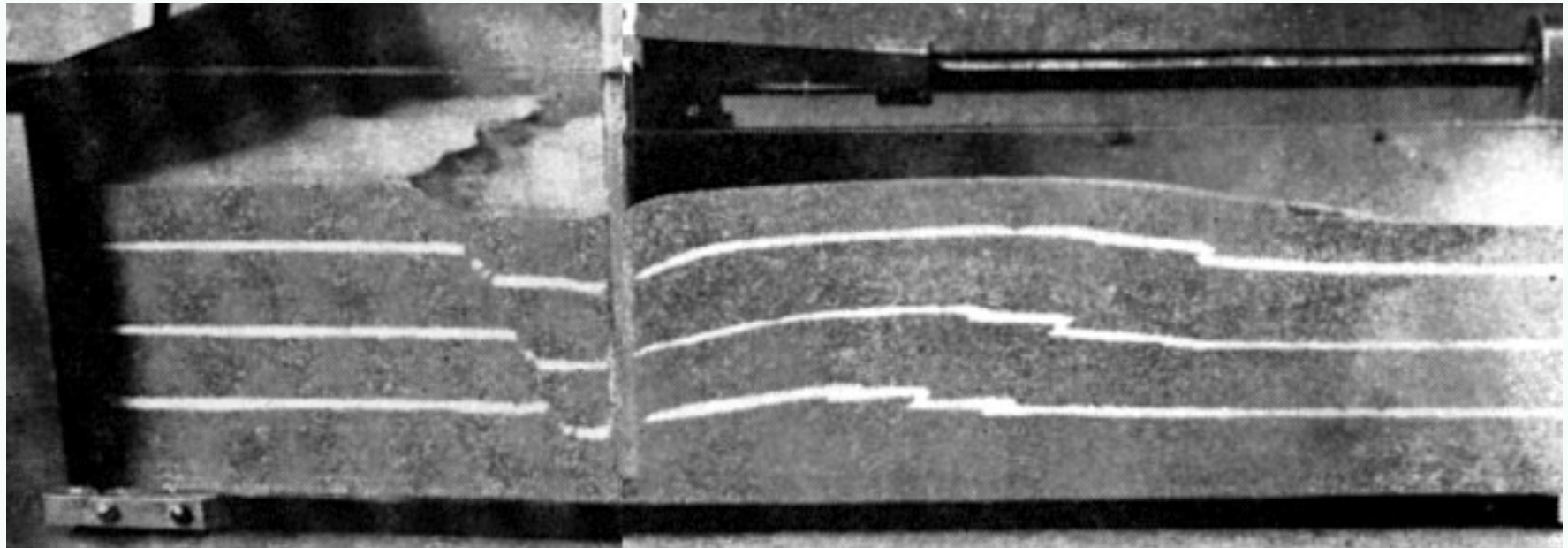
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- Two ways
  1. a constant regional stress can be added to one (or both) horizontal stresses over some vertical extent
  2. assume some regional strain which then generates a different stress in each layer, according to its stiffness
    - allows component of stress proportional to Young's Modulus
    - shown to work effectively in many field cases





# Regional Strain \_\_\_\_ Produces Tectonic Stress \_\_\_\_



Tension

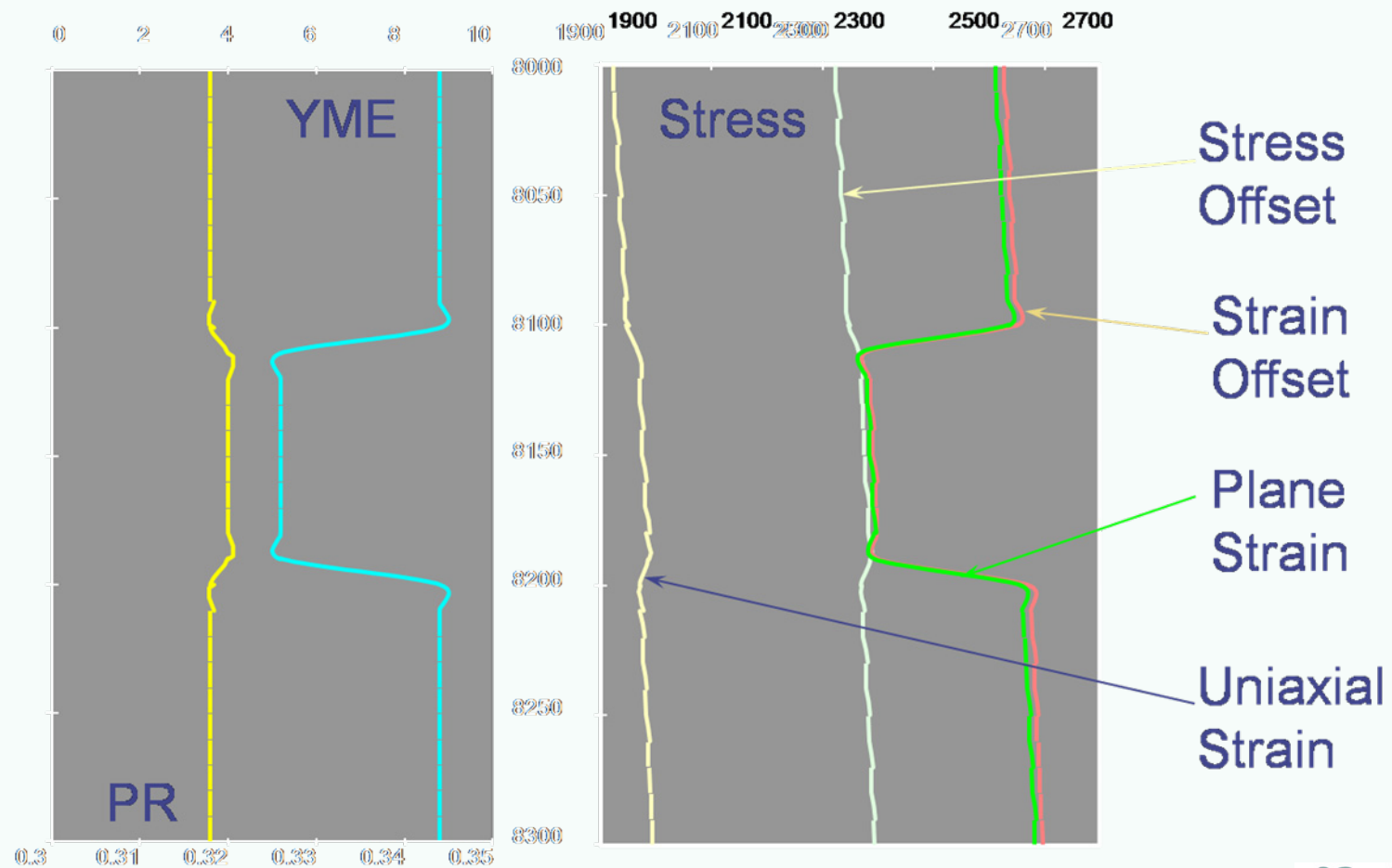
Regional Strain



Compression

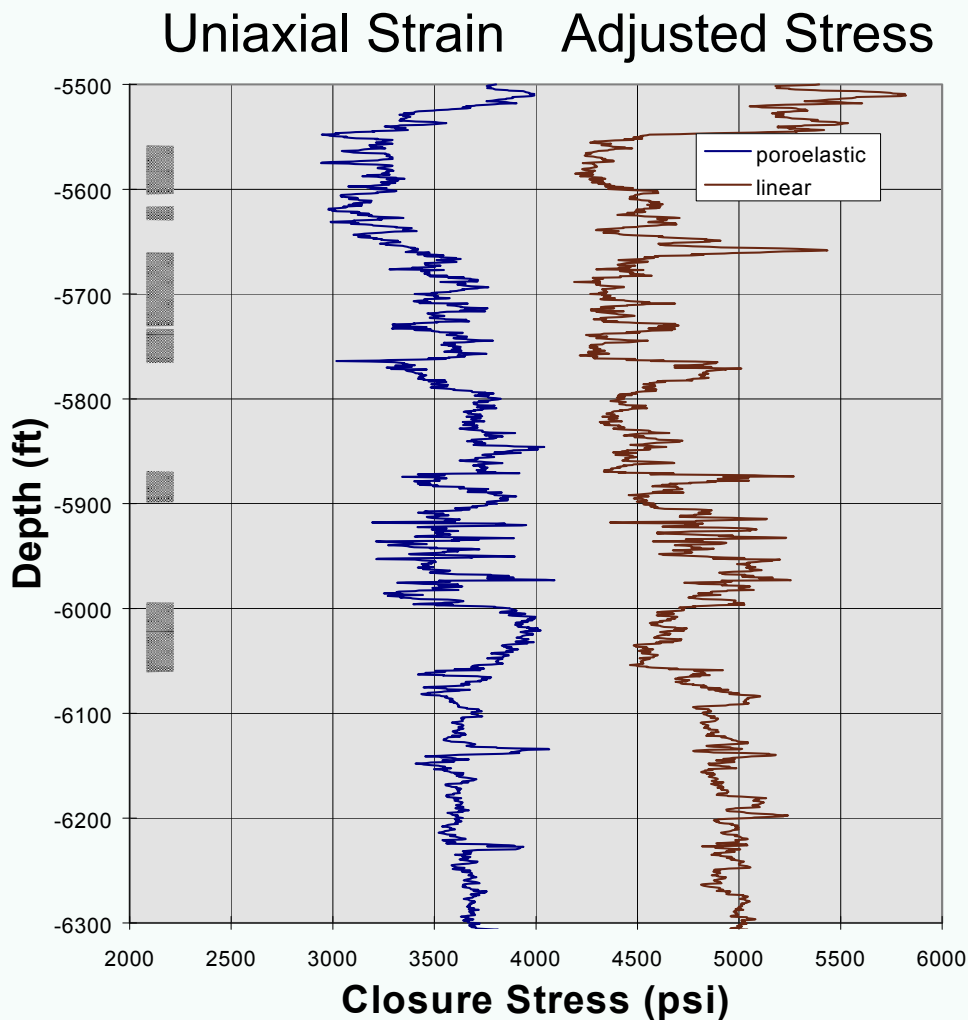


# Estimated Stresses Depend on the Model Used





# Stress Adjustments Through Tectonic Strain



*Added 200 micro-strains regional strain to stress calcs to match observed closure stress of 4500 psi at 6050'*



# GOHFER's Total Stress Equation

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We have now examined the various parts of the total stress equation:

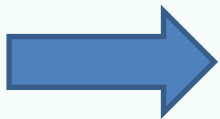
$$P_c = \frac{\nu}{(1-\nu)} \left[ D_{tv} \gamma_{ob} - \alpha_v (D_{tv} \gamma_p + P_{off}) \right] + \alpha_h (D_{tv} \gamma_p + P_{off}) + \epsilon_x E + \sigma_t$$



# Other Height

## Containment Mechanisms

- Inelastic energy dissipation
  - shear failure
  - bed slip
  - natural fractures
  - plastic deformation



Need to re-examine classical LEFM models  
(Linear Elastic Fracture Mechanics)





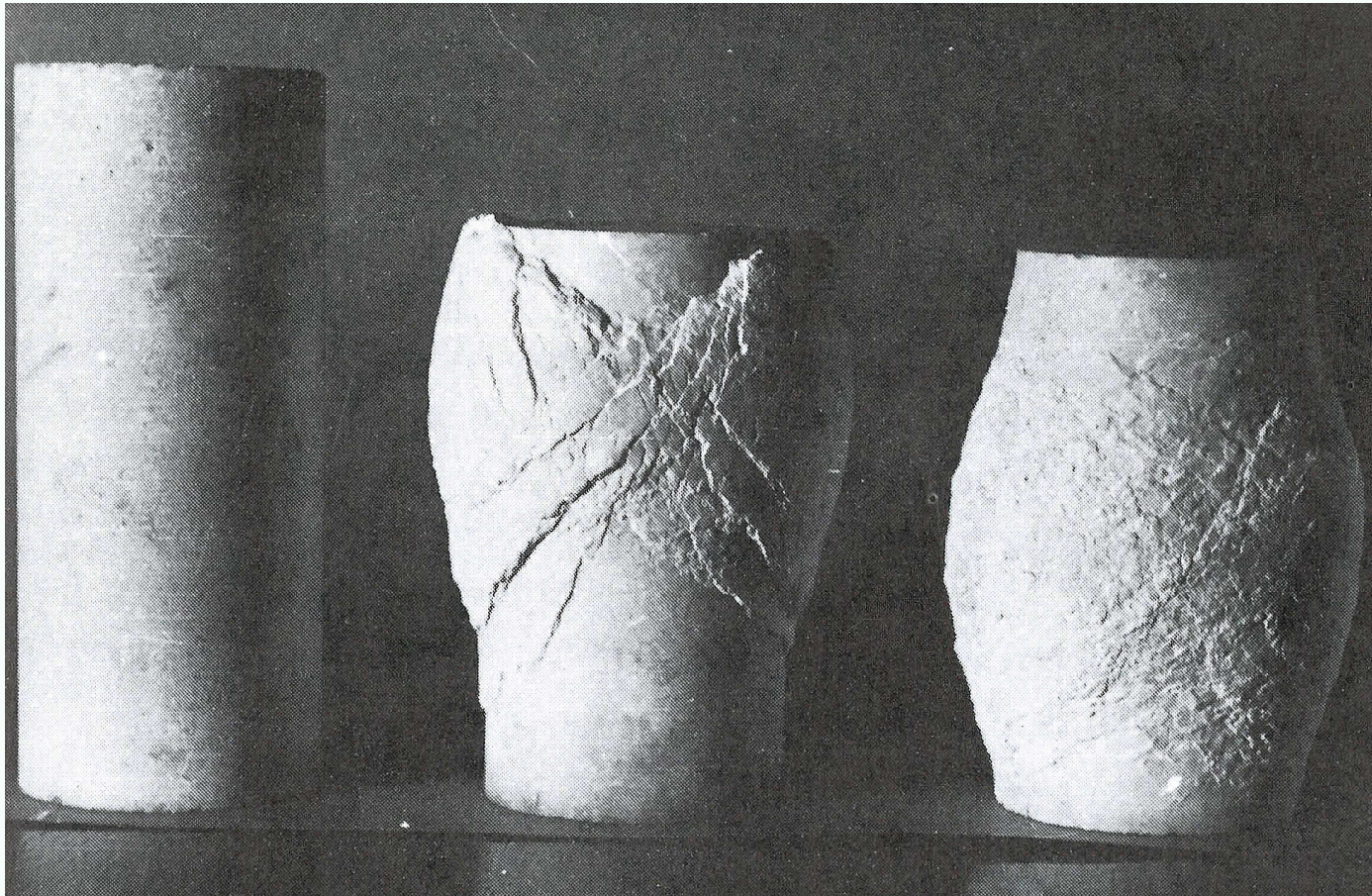
# Plastic Deformation of Rocks Under Confining Stress

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**Original Sample**

**4000 psi  
Confining Stress**

**6500 psi  
Confining Stress**

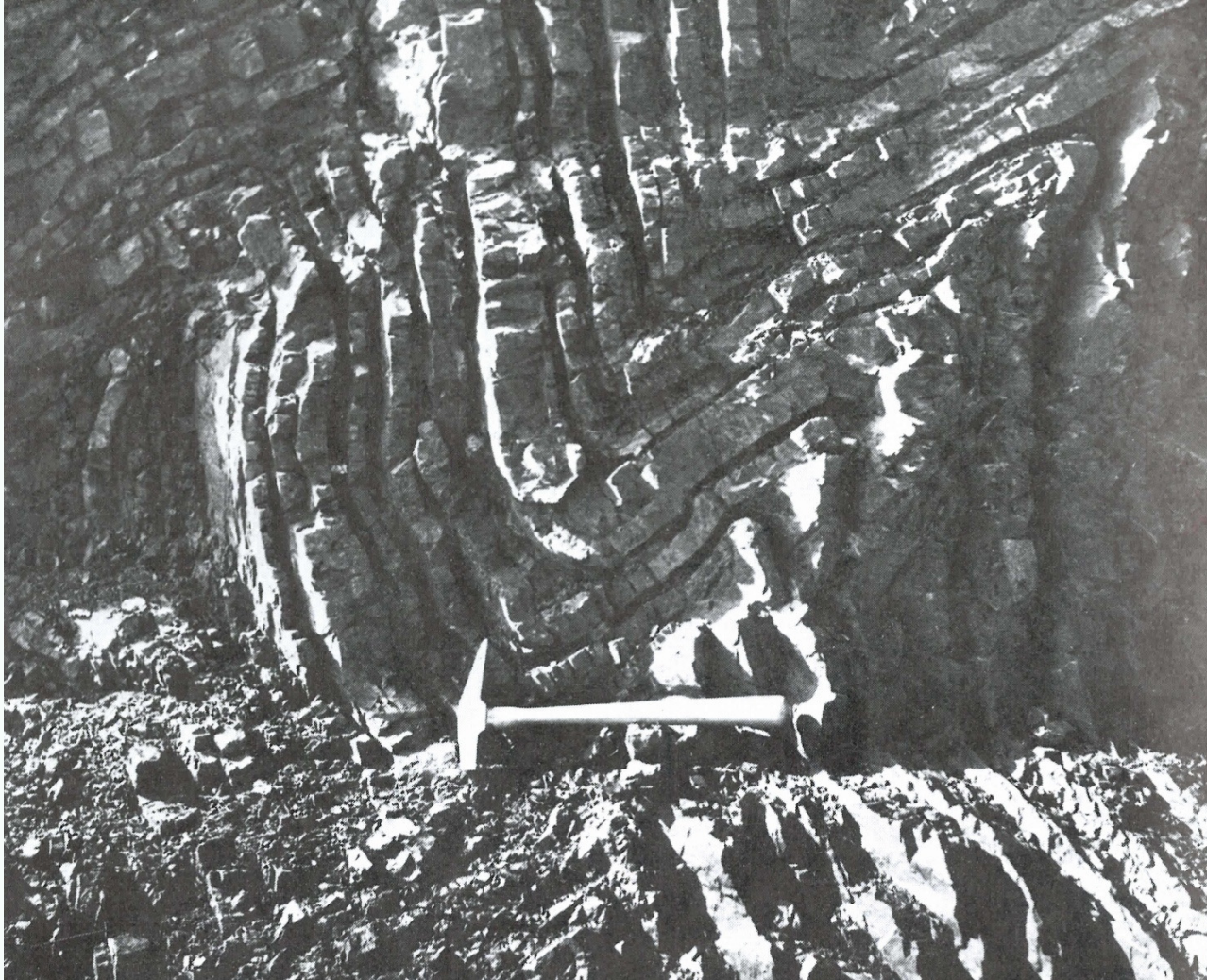






# Rocks Behave Like Plastic Materials

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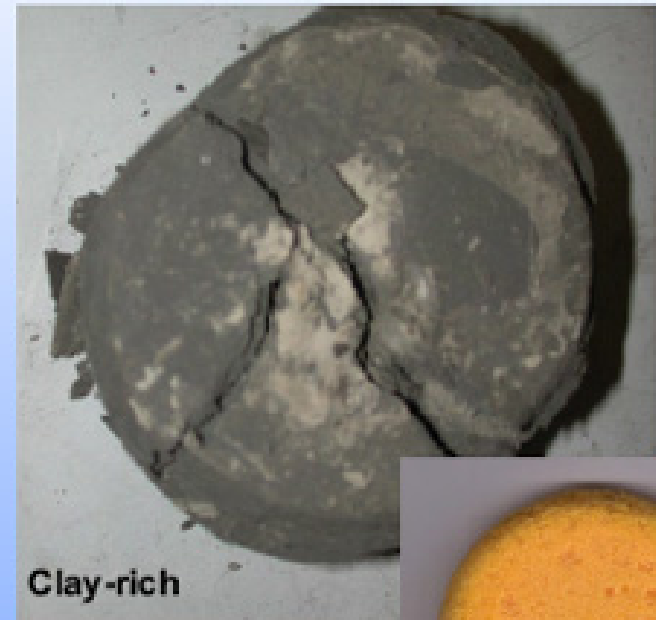


# Are All Shales the Same?

## Brittle vs. Ductile Behavior



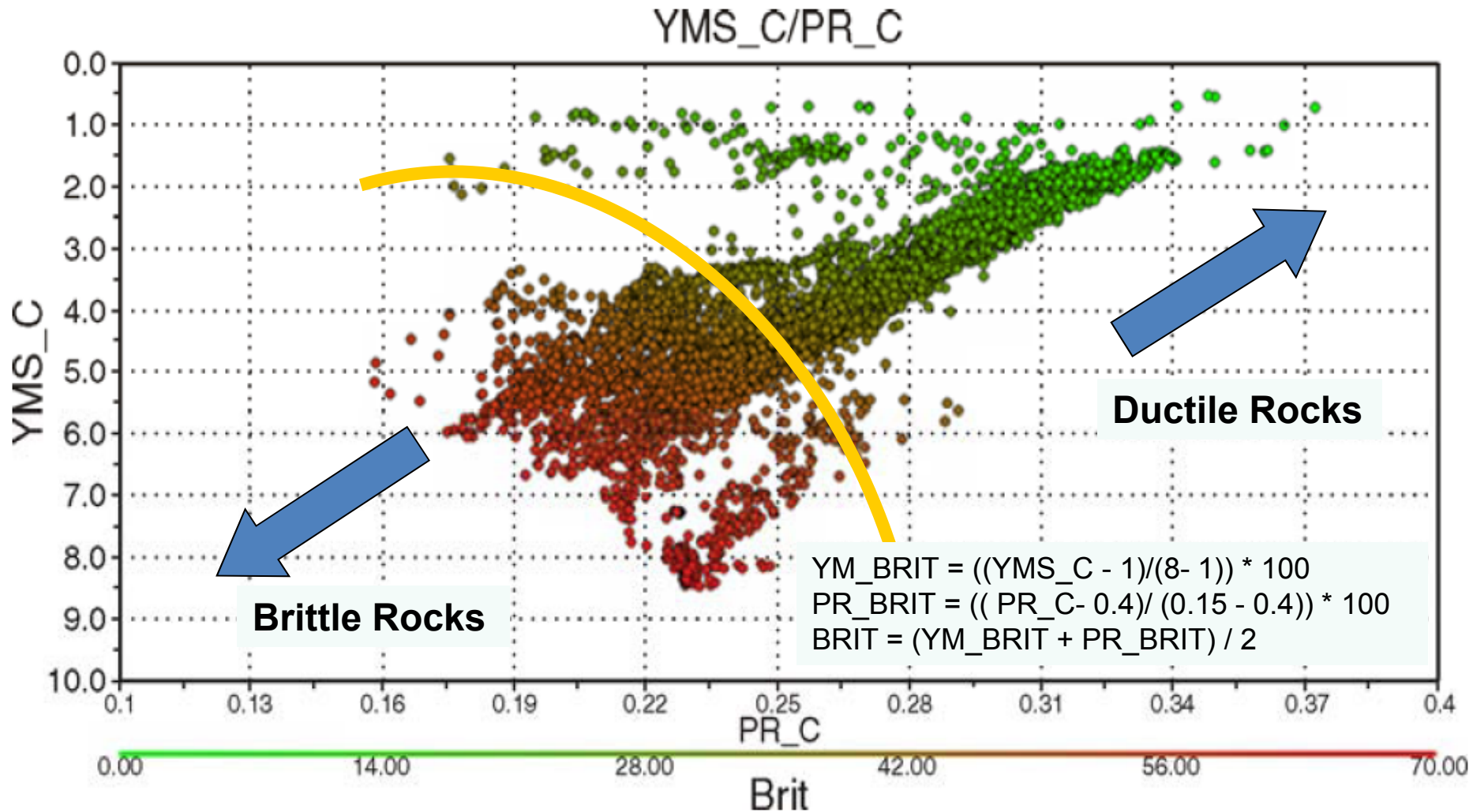
**Barnett Shale**



**Upper Cretaceous  
WCSB**

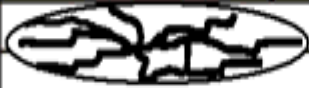




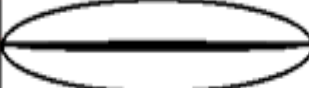



# Definition of Brittleness Based on E (YMS\_C) and $\nu$ (PR\_C)





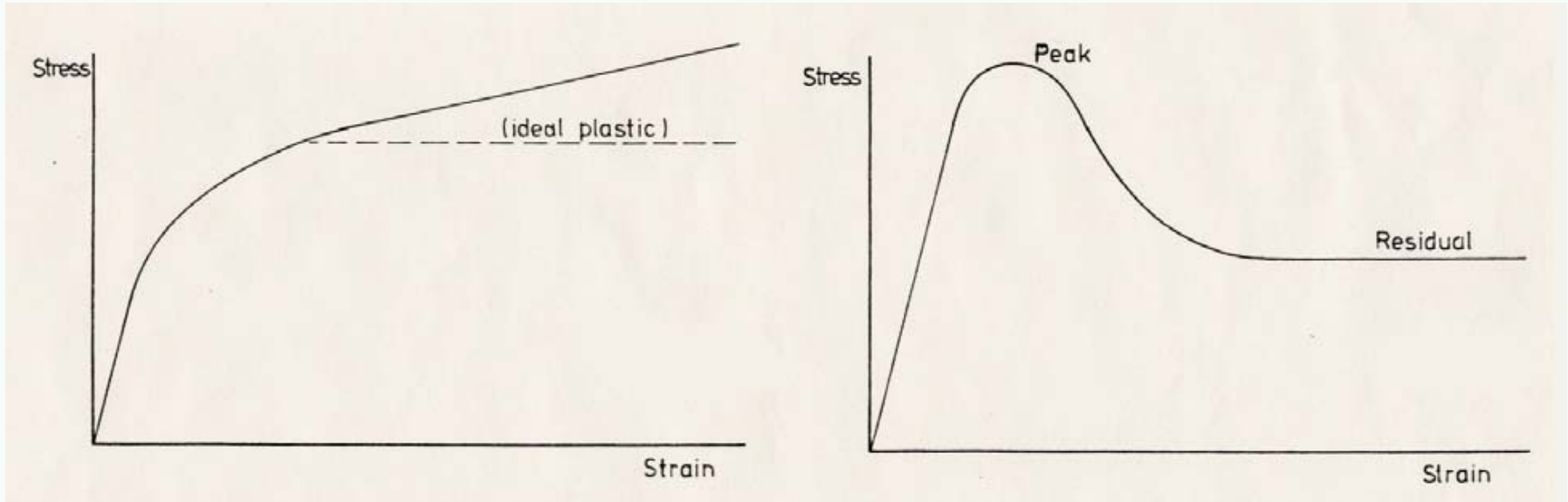
# Proposed Fracture Stimulation Choices Based on Brittleness

Brittleness	Fluid System	Fracture Geometry	Fracture Width Closure Profile	Proppant Concentration	Fluid Volume	Proppant Volume			
70%	Slick Water			Low	High	Low			
60%	Slick Water								
50%	Hybrid								
40%	Linear								
30%	Foam								
20%	X-Linked								
10%	X-Linked		High	Low	High				



# Definition of Brittle-Ductile Failure

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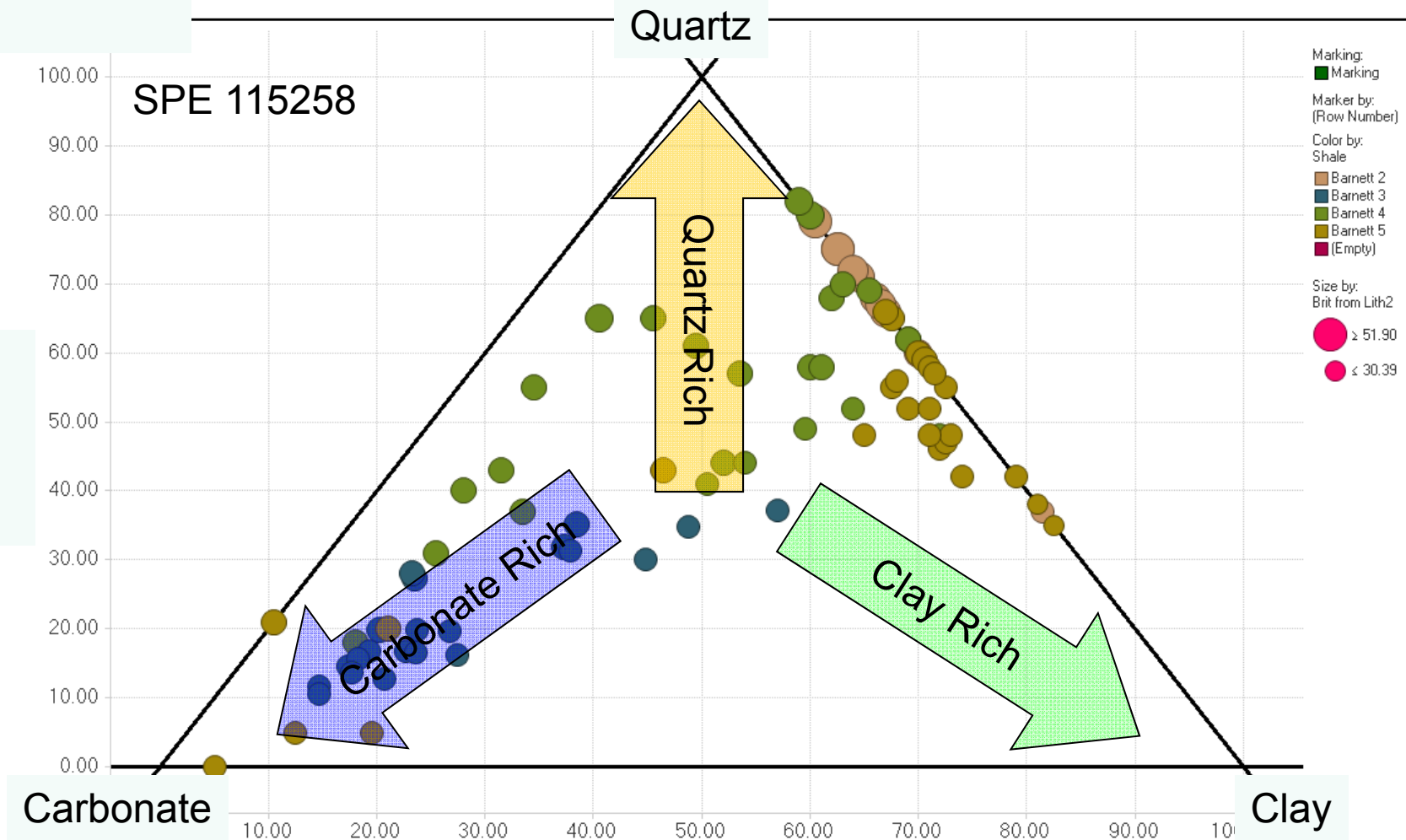


Quasi-plastic or strain-hardening

Brittle failure or strain-softening

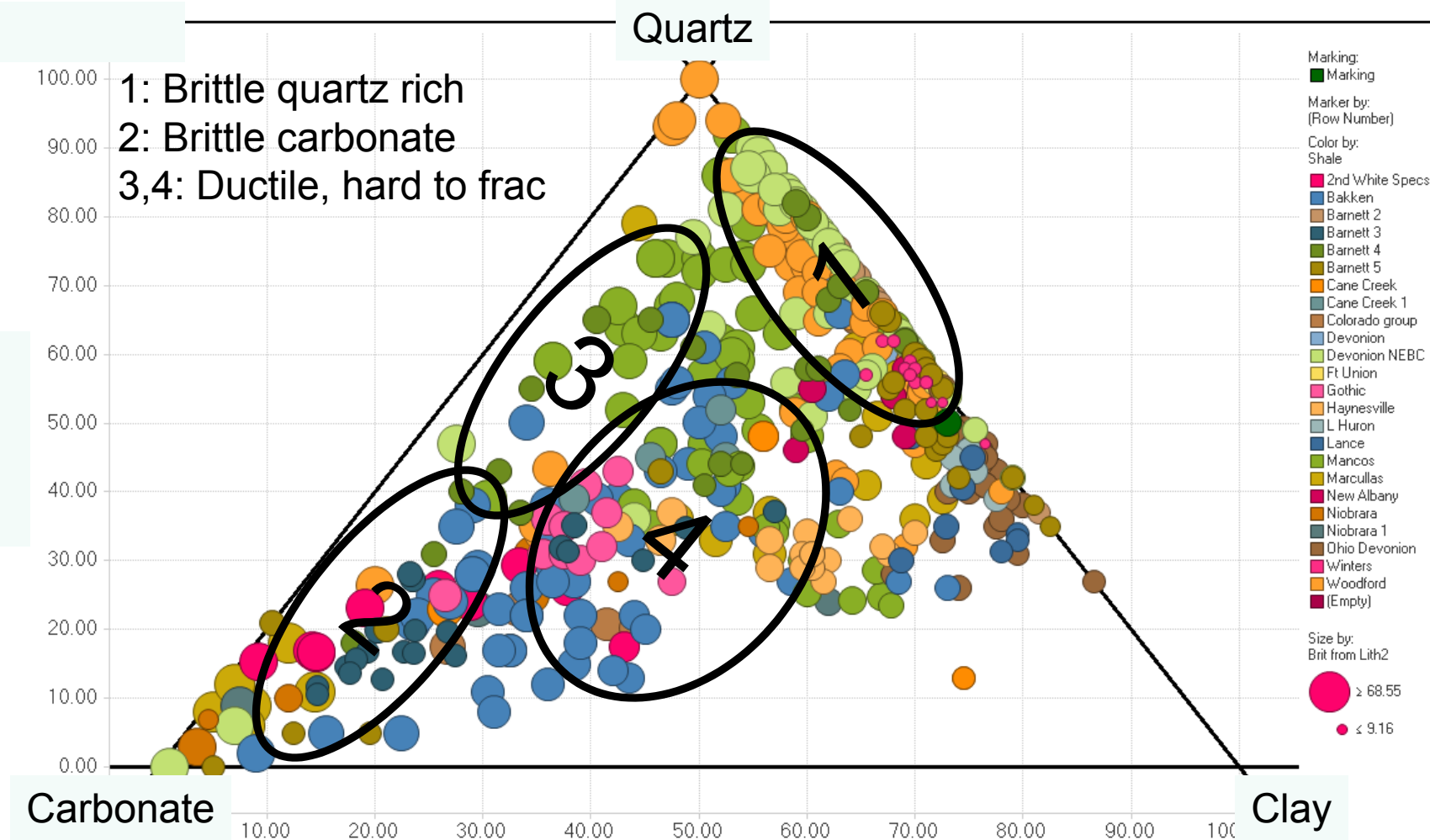


# Ternary Diagram of the mineralogy of four Barnett Shale Wells





# Ternary Diagram of the mineralogy of all Shales in the North America Database





# Plasticity and Creep:

## Effects on Stress Estimates

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- Apparent Poisson's Ratio approaches 0.5
- Horizontal stresses become nearly equal
- Horizontal stress can almost equal vertical stress
- Tendency for strong height containment in clay-rich, plastic sediments
- Possible blunting or fracture truncation



# Lithologies Susceptible to Plastic Creep

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- Coals
- Carbonates (at great depth)
- Gumbo Shales
- Evaporites
  - Halite
  - Anhydrite



# Confirming Input Data Accuracy

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- Need direct mapping of fracture growth
- Most data suggests that containment is much better than expected
- The stress model used is at least as important as the input data
- Elastic properties derived from sonic logs may not be the most useful
- Surrogate properties may give more predictive results
- Poroelasticity is important and may give a time and permeability dependence on apparent stress
- Assuming  $\alpha_v$  (PHIE) and  $\alpha_h=1$  gives the largest stress contrast in most systems
- Often other containment mechanisms must be invoked (shear-slip and layered media)